

MANATEE COUNTY UTILITIES

SOUTHEAST REGIONAL WATER RECLAMATION FACILITY: ELECTRICAL MASTER PLAN

FINAL JULY 2018

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MANATEE COUNTY UTILITIES

NORTH REGIONAL WATER RECLAMATION FACILITY ELECTRICAL MASTER PLAN

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1.0 EXECUTIVE SUMMARY

Manatee County (County) owns and operates the Southeast Water Reclamation Facility (SEWRF), an advanced wastewater treatment facility permitted to treat 11.0 million gallons per day (mgd) at a three month rolling average daily flow (TMRADF). Located in southeast Manatee County at 3525 Lena Rd in Bradenton, FL, the SEWRF was built in 1989 and serves as one of three water reclamation facilities for the County's service territory, treating County wastewater to reuse standards and pumping its effluent to a piped network of agricultural users. Influent treatment and effluent distribution have the capacity to demand several megawatts of electricity, and this load is expected to increase as the Manatee County population grows. This growth and the natural deterioration of aging equipment drive the need for continuous plant maintenance and improvement, and for that purpose the County has hired Carollo Engineers, Inc. (Carollo) to develop an Electrical Master Plan that guides this development. In it, Carollo assessed the plant's condition and proposes projects to maintain reliable service and manage growth wisely.

Carollo has investigated the following aspects of the SEWRF's existing plant and operations:

- Condition assessment of all major electrical gear, including: the physical integrity and operability of the enclosure, doors, switches, indicator lights, and overcurrent protection; the age and remaining life of equipment; the availability of spare parts, the impacts of a corrosive environment; spare electrical capacity; and physical space available to accommodate growth.
- The reliability of the plant to receive, treat, and discharge influent. Electrically, this means that the architecture of the electrical system accommodates the staff's needs to balance plant loads across distribution sources, minimize single points of failure, provide switching capability among distribution paths, and make alternate power sources available throughout the plant.
- The safety and functionality of the facility's electrical power system and distribution equipment in normal and abnormal conditions; whether the equipment operates within its ratings; arc flash conditions, operating procedures, and maintenance practices, the equipment's ability to isolate short-circuit faults; or whether equipment can be taken out of service for maintenance or repairs. This task included a review of the 2015 Electrical System Study and the recommendations that were made as a part of that study.

- The perspective of plant staff on equipment and systems that need repair or replacement, based on their experience with functionality and failures. Staff shared their concerns about equipment that poses safety hazards, operational inefficiencies, and maintenance liabilities. Their working experience with the SEWRF systems is consistent with Carollo's observations, and this report reflects their expertise and priorities just as it reflects Carollo's observations and judgment.
- An analysis of the SEWRF's utility service from Florida Power & Light (FP&L), including: reliability data at the plant's service entrances; billing data, by month, to build a 5-year energy profile of seasonal consumption; and a study of billing rates to determine the base rate, peak (kW) demand rate, and energy (kWH) rate for each service.

Having investigated the SEWRF plant and operations, Carollo then made recommendations to address existing deficiencies and potential problems that can be anticipated from the years 2018 to 2045. In terms of priority, Carollo recommends that the County first implement the Operational Improvements, as they have the potential to impact the quality and cost of all subsequent work. Second, Carollo recommends that the County implement the Short Term Improvements identified in Section 6. Finally, Carollo recommends that the County execute the Capital Improvement Projects identified in Section 7, in the order indicated. The recommendations are summarized as:

- Operational Improvements to improve safety, reliability, and minimum overall cost of ownership:
 - establish a stricter practice of maintaining plant documentation;
 - create a tagging system with unique identifiers that match field labeling to drawings;
 - define plant technical preferences, standards, or requirements for Electrical, Instrumentation, and Control installations (to simplify contracting and oversight of Consultants and Contractors;
 - develop an Electrical Preventive Maintenance (EPM) program that's aligned with NFPA 70B;
 - implement the Electrical Safety Plan (ESP) that Carollo provided in 2017;
 - record power meter data annually and reset meter fields (or have the data historized in SCADA and displayed on the HMI);
 - establish a procedure for taking an annual energy baseline.
- Short Term Improvements to secure the functionality of existing equipment that may be in use for many years.
- Capital Improvement Projects (CIPs) to maintain the plant's ability to treat and deliver water. Some of these projects are driven by the natural life cycle of electrical

equipment (whose materials degrade with time), some projects accommodate work being done on treatment processes, and others are recommended to match the system architecture to the evolving needs of the process. The goal is to build a resilient system at minimum overall cost to both capital and operational budgets.

1.1 Summary of Findings and Recommendations

Carollo's assessment of the SEWRF electrical distribution system (refer to one-line diagram EMP-2018) revealed that:

- The current configuration makes the plant power system vulnerable to a loss of either FP&L transformer, because SWGR-2A/B is mostly dedicated to process loads and SWGR-1A/B to effluent loads (with some overlap). Carollo proposes rearranging this configuration to dedicate each service transformer to one wing (load bus) of the replacement SWGR-1A/B. To clarify: when this report refers to SWGR-1A/B, it's referring to the existing switchgear, SWGR-1, which does not have a transfer bus (see the next paragraph for discussion of its replacement: SWGR-1A/T/B).
- The plant appears to be overinvested in standby power capacity, with 6000 kW (7200 kVA) of generator power available, but only 3000 kVA of utility transformer capacity. Some of that excess capacity will be required for starting your motors, but the largest motors are all run from VFDs so providing twice the generator capacity as transformers is excessive. Carollo recommends replacing the two separate generator switchgear assemblies with a single one that enables the plant to parallel its standby sources. The replacement SWGR-1A/T/B will have metering that allows staff to study the plant's loading patterns before deciding whether to replace Generators 1 and 2, both due for replacement in 2025. As an alternative, metering can be added before the replacement of SWGR-1A/T/B, and can provide valuable data to inform those projects. To clarify: when this report refers to SWGR-1A//T/B, it's referring to the new switchgear that will replace the existing SWGR-1A/B. The difference is that the new switchgear will have a transfer bus for receiving generator power added before.
- The original equipment, installed between 1988 and 1989, is reaching the end of its useful life. Numerous pieces of electrical equipment are obsolete due to changes in electrical technology and a lack of spare parts; others are in poor condition from 30 years of service. To maintain a reliable and safe power distribution system, electrical equipment more than 25 years old should be replaced in the next five to ten years (2023-2028).
- The overall load for the plant cannot be determined for several reasons: historical metering is absent from SWGR-1A/B, the co-generation system (Co-Gen) connects directly to SWGR-2A (limiting the value of service entrance data at SWGR-2A), and the meter on SWGR-2B is broken. By replacing SWGR-1A/B as recommended, the

overall plant load can be determined. Integration of the Co-Gen system with the remainder of the plant is outside the scope of this study.

Co-generation complicates any load study. A potential solution to this complication is to receive metering data from the SWGR-1A/B and the co-generation source at the HMI system and sum them internally for historical tracking and trends. In the short term, a rough estimate of overall plant demand can be measured at the meters on the backup generators. Unfortunately, the generators failed when we tried that during the project.

Recommendations for upgrading the power distribution system are summarized below (in Table 1), and an accounting of each cost estimate is further itemized in Sections 6 and 7. All numbers are given in 2018 dollars.

Tab	Table 1 Summary of Electrical Improvements and Related Construction Cost						
No	Description	Recommended Year	Total*				
0	Short Term Improvements	2019	\$159,000				
1	Replacements with RAS/WAS System Rehabilitation	2019	\$763,000				
2	Dedicated Plant Drain Station	2019	\$89,000				
3	Replace SWGR-1A/B and Generator Switchboards 1/2 and 2/3	2019	\$1,408,000				
4	Replace MCC-5 and MCC-6 (and Arc Flash Mitigation)	2019	\$683,000				
5	Anoxic Basins Mixer Replacements	2020	\$399,000				
6	Flow Equalization Tanks and Mixed Liquor Splitter Box Rehabilitation	2021	\$110,000				
7	Replace BFP control Panels with Belt Filter Press Upgrades	2022	\$394,000				
8	Secondary Clarifiers Rehabilitation	2022	\$65,000				
9	New MCC and Electrical Building for Anoxic/Aeration Basin #4	2026	\$776,000				
10	Electrical System Upgrades	2030	\$2,444,000				
11	VFD Replacements for Sludge Pumps	2033	\$90,000				
12	MARS Equipment Replacements	2035	\$1,273,000				
13	Replace Generator 1 in 2035	2035	\$1,833,000				
14	Biosolids Equipment Replacements	2038	\$585,000				
15	Replace Generator 2 in 2045	2045	\$1,833,000				
16	16Electrical Equipment Replacements2045\$415,000						
	OPINION OF TOTAL PROBABLE CONSTRUCTION COST \$13,319,000						

* Class 5 estimates, based on AACE.

2.0 CONDITION ASSESSMENT, GENERAL

These observations either apply to the incoming utility service or to the system as a whole. They involve assessments of equipment condition, but apply as condition trends across the plant, rather than isolated to a particular piece of equipment.

2.1 Power Supply from external sources: Utility and Co-Generation

FP&L supplies power to SEWRF at 480 volts (V), by way of two 1,500 kVA transformers that are both connected to the same FP&L circuit. The service transformers are located in a utility vault room within the Electrical Building, adjacent to the main Electrical Room where the main circuit breakers are housed. Each of the transformers supplies one assembly of low voltage switchgear with two circuits of service conductors: each circuit connects to one side of the switchgear (which has two buses, A and B, separated by a tie circuit breaker). Refer to drawing EMP-2018 for an Overall One Line Diagram of the existing plant.

Five-years of outage data from your FP&L feeder reveals that momentary outages (less than 60 seconds) peak at 2.4 outages/month from May through September (during storm season), while they average 0.5 outages/month for the rest of the year. In total, the SEWRF experiences about 18 momentary interruptions per year. Sustained outages (more than 60 seconds) occur at 0.6 times per year, lasting for about 0.5 hours. The sustained outage pattern is low, relative to other FP&L customers in the same service territory, and the pattern of momentary interruptions is high (perhaps due to lightning strikes at the neighboring landfill, which is the tallest land for miles).

A second power supply is provided from an independent power producer, SCS Energy of Long Beach, CA, who owns and operates an onsite generator that burns methane from the neighboring landfill. The co-generation system (Co-Gen) provides a relatively constant output (1400 - 1700 Amps; or 1200 - 1600 kW) of inexpensive electricity to the SEWRF. However, this power source is non-islanding and only generates when connected in parallel to FP&L and therefore cannot be used as a standby power source.. Standby power for outages is provide by diesel engine generators, as discussed below, and the reliability of the Co-Gen system is outside the scope of this study.

2.2 System Architecture: Switchgear, Generators, & Gen Switchgear

The architecture of the SEWRF's power distribution system organizes its loads mainly by utility transformer, grouping most of the treatment process loads on SWGR-2A/B and most of the effluent pumping (MARS) loads on SWGR-1A/B (though this distribution philosophy isn't applied consistently). Separate from SWGR-1A/B and SWGR-2A/B there are four circuit breakers connected to the three generators, with Generators 1 & 2 providing standby power for SWGR-1A/B and Generators 2 & 3 providing standby power to SWGR-2A/B (see drawing EMP-2018).

Carollo disfavors this arrangement because the configuration creates an unnecessary dependence on each of the utility transformers, because failure at either transformer eliminates the availability of utility power at one of the switchgear line-ups and all of its associated loads. Standby power from the SEWRF's generators is still available during a transformer failure, but the utility service would be more reliable for the plant as a whole if both utility transformers came into the same switchgear: One transformer dedicated to each side of a split-bus switchgear. An arrangement like this would also have more operational versatility - and it would be better able to distribute power from standby generators and Co-Gen.

Currently each switchgear line-up has a dedicated standby generator (Generator 1 for SWGR-1A/B and Generator 3 for SWGR-2A/B), additionally both switchgear line-ups are capable of receiving standby power from Generator 2 (see drawing EMP-2018). Generator 1 connects to SWGR-1A/B through a dedicated generator breaker. Similarly Generator 3 connects to SWGR-2A/B through a dedicated generator breaker. Generator 2 has 2 breakers one that connects to SWGR-1A/B and the other connects to SWGR-2A/B. None of the generators are paralleled to one another. Generator 1 is capable of supplying all SWGR-1A/B demand load (if the tie breaker is closed), similarly Generator 3 is capable of supplying all SWGR-2A/B demand load. Generator 2 can supply power to either or both SWGR-1A/B or SWGR-2A/B up to it rating; however, if Generator 2 was to simultaneously supply power to both SWGR-1A/B and SWGR-2A/B the plant staff would have to monitor its loading and manually shed load in order to not overload the generator.

While this arrangement is effective at providing sufficient standby power to plant loads, it does so expensively, requiring the plant to maintain 6000 kW (7,500 kVA) of generator capacity for processes that are adequately supplied by 3000 kVA of utility transformers. A simpler, less-expensive arrangement would integrate two generators at a single assembly of generator switchgear, rather than maintaining three generators and two generator switchgears. A single assembly of paralleling generator switchgear, if connected to a transfer bus (between the two load bus wings of the switchgear), could make standby power from two generators available to run the entire plant. Deferring the replacement of Generators 1 & 2 would save the County a lot of money, and avoiding the replacement of Generator 3would save the County ~\$1.5 million dollars.

2.3 System Architecture: Redundancy Loops between Twin MCCs

SWGR-1A/B and SWGR-2A/B directly power large VFD-driven loads. The remainder of distribution circuits from SWGR-1A/B and SWGR-2A/B feed motor control centers (MCCs), which in turn power process loads, building loads, and panelboards. This type of power distribution system is termed "radial." The alternative to "radial" distribution is "loop" distribution, where power is distributed from two breakers in the switchgear through a series of switches with taps for feeders between them. The "loop" distribution system essentially provides two sources of power to each load. Radial connections are simple, inexpensive,

and less reliable; loop connections are more complex, expensive, and reliable. While the SEWRF uses radial supply between service switchgear and MCCs, it does establish loop redundancy by connecting "twin-pairs" of MCCs together through a tie circuit breaker.

The benefit of the SEWRF's existing distribution system is that it gives each pair of MCCs (MCC-1 & 2, 3 & 4, 7 & 8, and 11 & 12) are supplied from two feeder circuits, when the Ties are cloased. For example: MCC-1 has one feeder from SWGR-2A; MCC-2 has one feeder from SWGR-2B; and a tie between the two MCCs gives either one access to either side of SWGR-2. Each paired MCC is normally supplied from opposite sides SWGR-2, and neither of these MCCs may be powered from SWGR-1 (or its FP&L transformer or Generator 1).

Redundant feeder circuits powering paired MCCs that have a tie breaker address some of the single point of failure concerns. The standby engine generators in conjunction with their associated FP&L transformers address the other single point of failure concerns. However, additional reliability could be achieved by sizing each FP&L transformer to power the entire plant load with each feeding separate ends of the same switchgear with tie breakers in between as depicted on EMP-2019. The replacement of SWGR-1A/B introduces this opportunity, and our recommended solution is explained below in the description of that project.

2.4 System Architecture: Co-Generation and Biosolids

The Co-Gen system is connected to the A-bus of SWGR-2A/B. It's not clear to Carollo how this system is integrated into the control, metering, and protection scheme of SWGR-2, but we see some problems with the configuration. First of all, it appears that the Co-Gen circuit breaker is intended to protect SWGR-2A at its ampacity (3200 A), but that its current transformer (CT) measurement is not summed with the CTs on its FP&L input at the Main Circuit Breaker to bus SWGR-2A (which is set for 3000 A). As such, it's possible that the process could draw current in excess of the switchgear's 3200 A capacity. A second problem with the Co-Gen system is that only SWGR-2A/B loads have access to it: if co-generation exceeds the loads on SWGR-2A/B and the County uses it at SWGR-1A/B, then the County would end up paying for the power twice: once from the Co-Gen supplier at SWGR-2/AB - and then again at SWGR-1A/B from FP&L (or possible at Biosolids MCC-1BSD, which is on a separate FP&L service entirely. We can't know when this problem occurs right now, because of the metering problems, but it might be happening any time Co-Gen supply exceeds the demand on SWGR-2A/B.

A third problem with the Co-Gen system, related to the second issue, is that the metering of the overall system does not give the plant accurate data for monitoring its loads. This is discussed further below, in Section 2.05.

Another aspect of the system architecture that's worth mentioning is that there's another service entrance in addition to the two FP&L services that were described above. The Biosolids Dryer building receives its own FP&L service directly into a 1600 A motor control

center. With its own, autonomous service, this building has no access to SEWRF standby capacity or less expensive Co-Gen power, and is inherently less reliable than the remainder of the plant (though this isn't a major concern though, as the Biosolids function is not critical). The arrangement is also problematic for having the service conductors connected directly from the utility transformer secondary to MCC-1BSD, because transformer secondaries have the most energy available for (and slowest protection against) arcing faults.

The County has expressed interest in having MCC-1BSD supplied from the same service switchgear as the rest of the plant, which would solve both problems (of having an upstream service disconnect and providing access to Co-Gen and standby generators). However, Carollo is concerned about available capacity at the service switchgear, which might be near 3600 A on a 4000 A bus, if its recommendations are followed to consolidate the service entrances into one assembly. As such, Carollo recommends that the County address its metering problems first to acquire a more accurate sense for the true demand load of the plant. If the data is favorable, then it might make sense to look at supplying MCC-1BSD from a new SWGR-1A/B.

2.5 Metering Problems at Switchgear

The overall load for the plant cannot determined for several reasons: historical metering is absent from SWGR-1A/B, the meter on SWGR-2B is broken, and the Co-Gen system connects directly to bus SWGR-2A without a local meter display (and this significantly limits the value of service entrance data at SWGR-2A). The Co-Gen system, in particular, complicates the metering scheme because it can lead to positive or negative flows through the main circuit breaker of bus SWGR-2A, and it's not clear that the two sources have been properly integrated to reflect the arrangement. This issue is problematic because the NEC sizing rules require that a project adding load demonstrate bus capacity by calculations (which presently indicate more connected load than switchgear capacity) or historical metering (which always has more favorable numbers than the sum of connected load).

Carollo recommends that a historical, digital meter be provided for each source (including generators and Co-Gen), that the data be received at the SCADA system, and that the sources for each bus are summed by SCADA for historical tracking and trends of power consumption at each switchgear bus.

2.6 Power Quality Problems at MCCs

Digital metering is present at 8 MCCs out of 16 total. These digital meters log historical highs and display measurements of power factor, harmonic current distortion, and harmonic voltage distortion. A survey of those meters found that power factor was low throughout the plant: the typical range was 0.75 to 0.85, with some buses as low as 0.25 at the time of observation. The harmonic content of voltage and current were low on most buses, in the

range of 1-3%, but the harmonic current on MCC-11 was found to be 35%, a very high value.

The measurements of low power factor can probably be attributed to the failure of power factor correction capacitors around the plant, leaving several large, across-the-line loads without a local source for their reactive power requirements. The measurement of high harmonic current at MCC-11 can be attributed to the two 75 HP, 6-pulse, variable frequency drives (VFD) for the RAS pumps, neither of which have a line reactor (or other harmonic mitigation). The County could address these problems by replacing (and maintaining) its failed power factor correction capacitors, installing of new 3% (min) line reactors for all VFDs, performing maintenance testing on your ground system, installation of digital power meters where they're not provided, and monitoring the power quality metrics with the existing meters.

3.0 CONDITION ASSESSMENT, ELECTRICAL EQUIPMENT

3.1 History of the SEWRF Power System

Carollo Engineers performed a condition assessment of the SEWRF's electrical distribution equipment, including a review of record drawings from the original construction in 1989, the major "WWTP Expansion" project in 2002, and the "10 MG Storage Tank & Interconnection" project in 2017. The following is a summary of the major electrical system projects completed or in construction since the 1989 construction:

- In 1989, the original plant was built with SWGR-1A/B (manufactured in 1986) supplying the entire process via MCCs, with one 750 kW generator connected to lugs on bus SWGR-1A. Original MCCs 1, 1A, 2, 2A (in 2002 and 2013) have all been replaced; original MCCs 3 and 4 were re-labeled MCCs 9 and 10 (in 2000); and original MCCs 5 and 6 are still in-service. Many original panelboards are also still inservice.
- In 1995, Generator 1, Generator 2, and Generators 1 & 2 Switchgear were all installed, connecting Generator 1 to bus SWGR-1A and Generator 2 to bus SWGR-1B.
- In 2002, the electrical system was expanded to connect new Effluent Pumps at SWGR-1A/B and provide SWGR-2A/B as the power source for several new MCCs to supply the equipment additions of the expanded process (present MCC-1, MCC-2, MCC-3, MCC-4, MCC-7, MCC-8, MCC-11, and MCC-12). Generators 2 & 3 Switchgear and Generator 3 were also provided at this time, realizing the switchgear configuration that's in place today.
- In 2007, the Biosolids Dryer building was added, with a new FP&L service to MCC-1BSD.
- In 2013, the co-generation system was connected to bus SWGR-2A, providing the plant with electricity generated from landfill gas.
- In 2016, the septage receiving station was installed, including new MCC-SEP that is fed from MCC-1.
- In 2017, the 10 MG storage tanks were commissioned, replacing the previous large effluent pumps with the new pumps for High Service (four pumps at 400 HP each) and Low Service (five pumps at 100 HP each). New MCC-13 & MCC-14 installed.
- 2018: refer to the Summary of the Condition Assessment, below.

3.2 Summary of the Condition Assessment of Electrical Equipment

Table 2 Condition Assessment, SEWRF Major Electrical Equipment					
Equipment	Function in Distribution System	Year of Manufacture, Physical Condition ⁽²⁾	Location	Action Recommended	
SWGR-1A/B	Service entrance switchgear. Supply for MCCs 9, 10, 5, & 6, and for 3 of 4 High Service Pumps,	1986 Poor. Hot spots found with thermal imaging (repaired 2016). No written procedure for switching operations. Door clasps loose and status lights out on a few cubicles.	Main Electrical Room	 Replace assembly as soon as possible. Replace both Generator Switchgear assemblies at the same time. Connect new Generator Switchgear to transfer bus of new SWGR-1A/B. Connect one FP&L transformer to each side of new SWGR-1A/B. Leave space for future additions, when it's time to replace SWGR-2A/B. Replace service entrance cables to SWGR-2A/B with new feeder circuits from new SWGR-1A/B. 	
SWGR-2A/B	Service entrance switchgear. Connection of Co-Generation Supply for MCCs 1, 2, 3, 4, 7, 8, 11, 12, & 13; and for 1 of 4 High Service Pumps,	2001 Good. Faulty meter 2B. Poor integration of Co- Gen circuit breaker. Mislabeling between protective functions and existing documentation.	Main Electrical Room	Repair or replace both power meters. Incorporate all power sources metering (utility, Co- Gen, and generators) into SCADA system for historical tracking. Replace service entrance cables to SWGR-2A/B with new feeder circuits from new SWGR-1A/T/B. Replace assembly in 2032 (as mentioned above for SWGR-1A/B). Replace or remove in 2032 (with additional vertical sections on SWGR-1A/B to supply loads currently fed by SWGR-2A/B).	

Table 2	Table 2 Condition Assessment, SEWRF Major Electrical Equipment					
Equipment	Function in Distribution System	Year of Manufacture, Physical Condition ⁽²⁾	Location	Action Recommended		
Generator 1	2000 kW Standby Power	1995 Good. Lightly used. Exercise is irregular. Staff has reported "generator batteries blowing up during a recent exercise." Carollo witnessed an electrical short circuit at the fuel day tanks during an exercise in May.	Generator Room	Exercise regularly. Keep up with routine maintenance. Have Ring Power perform in-depth technical analysis (including oil analysis and fuel usage) every 3 years. Replace generator in 2035.		
Generator 2	2000 kW Standby Power	1995 Good. Lightly used. Exercise is irregular.	Generator Room	tor Exercise regularly. N Keep up with routine maintenance. Have Ring Power perform in-depth technical analy (including oil analysis and fuel usage) every 3 yea Replace generator in 2035.		
Generator 3	2000 kW Standby Power	2001 Good. Lightly used. Exercise is irregular.	Generator Room	 Exercise regularly. Keep up with routine maintenance. Have Ring Power perform in-depth technical analysis (including oil analysis and fuel usage) every 3 years. Retire Generator 3 once Generators 1 & 2 are paralleled. This assessment should be re-visited once the plant's demand load pattern is verified. 		

Table 2 Condition Assessment, SEWRF Major Electrical Equipment					
Equipment	Function in Distribution System	Year of Manufacture, Physical Condition ⁽²⁾	Location	Action Recommended	
Generators 1 & 2 Switchgear	Connecting Generators 1 & 2 to SWGR-1A/B	1995 Good. Indicator lights out. Poor documentation of system and switching procedures.	Main Electrical Room	Replace with a new Generator Switchgear assembly (SWGR-GEN) for two of the generators at the same time as replacement of SWGR-1A/B. This may require generator modifications to the governors, governor controllers, and voltage regulators.	
Generators 2 & 3 Switchgear	Connecting Generators 3 & 2 to SWGR-2A/B	2001 Good. Poor documentation of system and switching procedures.	Main Electrical Room	Replace with a new Generator Switchgear assembly (SWGR-GEN) for two of the generators at the same time as replacement of SWGR-1A/B. This may require generator modifications to the governors, governor controllers, and voltage regulators.	
MCC-9, MCC- 10, MCC-5, and MCC-6	Supplies power to solids handling, filters, and two plant drain pump stations.	1986. Poor.	Belt Filter Press Electrical Room	Remove equipment and replace with new, including digital meters for each MCC.	
MCC-1, MCC-2, MCC-3, MCC-4	Supplies power to EQ basin, headworks, aerators, aeration basin mixers, RML pumping, and two plant drain pump stations.	2000. Good. Capacitors bad. NEC violation on OCP to MLR pumps.	Headworks /Aeration Basin Electrical Room	Repair or replace power factor correction capacitors. Replace motor circuit protectors on feeder circuit to VFDs (for MLR pumps) with molded case circuit breakers (for OL protection, in addition to short circuit). Replace equipment in 2030 (or sooner, depending on the 4th basin).	

Table 2 Condition Assessment, SEWRF Major Electrical Equipment					
Equipment	Function in Distribution System	Year of Manufacture, Physical Condition ⁽²⁾	Location	Action Recommended	
MCC-7, MCC-8, MCC-11, MCC- 12.	Supplies power to sludge thickening, filters, and two plant drain pump stations.	2000. Good. Mislabeling. Low power factor.	Headworks /Aeration Basin Electrical Room	Install power factor correction capacitors or VFDs for sludge blowers. Stock spare parts for auto-transformer starters on sludge blowers. Remove equipment and replace with new in 2030.	
MCC-1A, MCC- 2A	Supplies power to headworks and odor control	2013. Good. No power meters, but sub-fed from adjacent MCCs 1, 2 (metered).	Headworks /Aeration Basin Electrical Room	Replace equipment in 30 years - or possibly earlier when MCC-1 and MCC-2 are replaced (to consolidate space and update technology).	
MCC-13, MCC- 14	Supplies power to MARS system (low service and HS jockey pumps)	2015. Good.	MARS Electrical Room	Replace equipment in 30-years	
Panelboards & Transfer Switches	Supplies power to non-continuous loads for process & auxiliary loads.	Varies: 1989 - 2016 Varies: poor to good.	Throughout plant	 Maintain circuit breakers per NFPA 70B. Replace as indicated in project descriptions. Dry-type transformers can stay in-service for the lift of the building. 	
VFDs for RAS Pumps (3)	Separately- mounted VFD starters for RAS pumps	2000. Good.	Main Electrical Room	Replace these with the RAS/WAS rehabilitation schedule for 2018. When replacing, provide 5% line reactors and DC bus chokes to protect the VFDs from upstream voltage surges and mitigate harmonic currents.	

Table 2 Condition Assessment, SEWRF Major Electrical Equipment					
Equipment	Function in Distribution System	Year of Manufacture, Physical Condition ⁽²⁾	Location	Action Recommended	
VFDs for WAS Pumps (4)	Separately- mounted VFD starters for RAS pumps	2000. Good.	Main Electrical Room	Replace these with the RAS/WAS rehabilitation schedule for 2018. When replacing, provide 5% line reactors and DC bus chokes to protect the VFDs from upstream voltage surges and mitigate harmonic currents.	
VFDs for MARS (HS, HS Jockey, and LS Pumps)	Separately- mounted VFD starters for MARS pumps	2015. Good.	Main & MARS Electrical Rooms	Replace these in a "VFD Replacements Project" in 2035. When replacing, provide 5% line reactors and DC bus chokes to protect the VFDs from upstream voltage surges and mitigate harmonic currents.	
VFDs for RML Pumps	Separately- mounted VFD starters for RML pumps	2000. Good.	Gallery between Aeration Basins	RML pumps and VFDs will be demolished in 2020 with the Anoxic/Aeration Basins Enhancements project.	
VFDs for Sludge Thickening Pumps (301, 302, 303, 304, 306)	Separately- mounted VFD starters for sludge thickening pumps	2000. Good.	Sludge Thickening Electrical Room	Replace these with an Arc Flash Mitigation project or Electrical Upgrade project in the timeframe of 2019- 2020. When replacing, provide 5% line reactors and DC bus chokes to protect the VFDs from upstream voltage surges and mitigate harmonic currents.	
VFDs for Sludge Thickening Pumps (305, 307, 308)	Separately- mounted VFD starters for sludge thickening pumps	2013. Good.	Sludge Thickening Electrical Room	Replace these in a VFD Replacements project in 2035.	

Determinations of condition made by visual observation
 Additional specific assessment of each key electrical apparatus has been included with pertinent issues and recommendations and they are shown on figures with photographs in Appendix A.

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3.3 Equipment Vulnerabilities: SWGR-1A/B

Manufactured in 1986 by Westinghouse, service entrance switchgear SWGR-1A/B is past its useful service life. Staff spoke of "hot spots" that the service contractor found during thermal imaging in 2016, and the loose connections have been corrected. Visual inspections at the site visit also found door clasps loose and status lights out on a few cubicles. The existing circuit breakers are from the discontinued Westinghouse line of "SPB" insulated case circuit breakers, using Pow-R-Trip 7 digital trip units. The metering on these assemblies is only an analog voltmeter and ammeter that measures the instantaneous voltage and line current from FP&L. No historical data is available to indicate the peak demand load and the connected load is at the 3200 A capacity of the bus, so adding any load to this switchgear would require a load study in accordance with the requirements of Article 220 of the National Electrical Code. The battery charger and batteries for control power appear to be as old as the switchgear itself, and should be replaced with the switchgear.

Most of the SEWRF's effluent pumping capacity is supplied from SWGR-1A/B - although one 400 HP High Service Pump could still be run from SWGR-2A/B during an outage at SWGR-1A/B. Considering this, the age, and the condition of SWGR-1A/B, this switchgear represents a vulnerability to the reliability of SEWRF's mission to deliver treated wastewater for re-use. The tanks for 10 MG Storage mitigate the vulnerability somewhat, as the plant would be able to store treated wastewater during outages that disrupt its capacity to distribute to its re-use (MARS) network, but that's a short term solution to maintain a minimal amount of throughput. This switchgear should be replaced as soon as possible.

3.4 Equipment Vulnerabilities: SWGR-2A/B

Manufactured in 2001 by Cutler-Hammer and installed in 2002, service entrance switchgear SWGR-2A/B is DSII Metal-Enclosed LV Switchgear. The switchgear itself it in good working condition, with an undamaged enclosure that is free of corrosion. Being located in an air-conditioned space that's sheltered from weather and other damage, this assembly should be suitable to remain in service until 2032, when it should be removed for deteriorating insulation, less reliable overcurrent protection, corrosion on electrical contacts, and availability of spare parts. However, problems with this switchgear have been observed that should be corrected to enable it to continue functioning reliably for the remainder of its service life - particularly considering the critical role that this switchgear has in powering nearly all of the SEWRF wastewater treatment processes.

Staff have reported "hot spots" in SWGR-2A/B that were found by the service contractor during the annual thermal imaging that they perform (upstream of the feeder circuit to MCC-2), and the loose connections identified in these scans have been corrected. While thermal imaging is an important step of routine preventive maintenance, the SEWRF should also perform the cleaning, inspection, and testing recommendations of NFPA 70B and the equipment manufacturer.

Another concerning set of issues for SWGR-2A/B are the metering issues discussed above. In short, the Co-Gen supply has no metering that's visible to the plant, and for that reason it's impossible to know if the digital metering on the FP&L service to bus A of SWGR-2 represents the demand load or only the demand load that exceeds the Co-Gen supply. The digital meter on the FP&L service to bus B is defective and should be replaced. A short-term solution to provide better distribution for the Co-Gen power would be to operate SWGR-2A/B with the tie breaker closed and only the main circuit breaker to bus A closed.

Labeling errors were found on the meters and protective relays on the face of the switchgear. The Basler BE1-47N protective relay for "voltage phase sequence" is labeled as 24/47-2, though protective function 24 (Volts/Hertz) is not available on the relay - while undervoltage (27) and overvoltage (59) protection both are. Likewise, the power meter is labeled 27/47-2, though it's doubtful that this relay is integrated to provide protective functions. Errors were found in the existing documentation compared to the factory drawings for this switchgear, but the new set (provided with this Electrical Master Plan) has been corrected.

3.5 Equipment Vulnerabilities: Generators 1, 2, & 3

Cummins manufactured Generators 1 & 2 in 1995 and Generator 3 in 2001. Carollo's investigation into generator operation was limited due to equipment failures and the availability of switching procedures, but those observations themselves are instructive.

During a generator exercise in May 2017, Carollo witnessed an electrical short circuit occurring in the fuel day tanks for two of the three generator units. These equipment failures were not an isolated incident, as staff reported an event of having the generator batteries "blow up" recently during a generator exercise. These problems with the generator system auxiliaries indicates that generator maintenance is not being kept up and that the units are not regularly exercised. For maintenance, inspections should be performed and levels should be replenished for lubrication, cooling, fuel, battery, and exhaust systems. Manufacturer's recommendations should be referenced for more detailed on maintenance practices.

Generator exercising, though performed under plant load, has not been performed consistently. Staff reported that they did not exercise the generators for a long time, but had recently resumed the practice. The renewed practice involved a schedule of running two of the three generators each month (units 1 & 2 in one month, 2 & 3 in the next month, 3 & 1 in the following month, etc). Monthly exercise is critical to keep engine parts adequately lubricated, inhibit oxidation of electrical contacts, and use fuel before it deteriorates.

Co-Gen only works when the plant is connected to FP&L; the Co-Gen system is not designed to parallel with the plant's standby generators. Conversely, the standby generators do not parallel with the utility, and transitions between standby generators and FP&L are open (with no overlap period to maintain power for the facility when the switching from utility power to standby - or vice versa). This transition to and from standby generators is a fundamental aspect of operating the equipment that the operators should be aware of, and which should be reflected in detailed operating procedures. When Carollo tried to perform a routine generator exercise on-site with

plant staff, a written operating procedure wasn't available and we had to call a retired, former employee, to proceed. This substantiates that periodic exercising of the standby generators has not been occurring. A written operating procedure was discovered after Carollo left, but it should be easily available to plant staff (and it included inadvisable directions, such as exercising one generator without load each month - which conflicts with manufacturer recommendations).

While the generator problems discussed above undermine the reliability of the SEWRF's standby power supply, a palliative to this vulnerability is that the plant has 6000 kW of generator capacity to dispatch from three units. This makes it more likely that at least two units will be available to serve when called upon. The County's local Caterpillar representative, Ring Power, reports that these generators can stay in service for 40-50 years (or more; they have old machines in-service that were installed in the mid-1960s). Each of the three SEWRF generators are Caterpillar's model 3516, which is one of their most popular models - with widespread availability of spare parts expected far into the future (product obsolescence is not foreseen at this point). Ring Power advises that, to achieve that kind of longevity from its generators, the County's maintenance plan for these units should follow Caterpillar guidelines.

Considering Ring Power's perspective, Carollo's first recommendation regarding the generators is that the County maintains these units to get 40 years of service from Generator 1 and 50 years of service from Generator 2. In addition to the diligent maintenance recommended above, the County should have Ring Power perform an on-site, in-depth technical analysis on all of its generators. This inspection should include oil analysis and a retrieval of fuel usage data from the generator's on-board controller. This data enables them to see how hard the machine was driven and identify any engine problems before they become detrimental. If this strategy is pursued, the County could expect to replace Generator 1 in 2035 and Generator 2 in 2045.

While Generator 3 is younger than the other two units by 6 years, its internal windings have a different pitch than units 1 and 2 - making it more difficult to parallel them together (as recommended below). With the plant's largest motors all run from VFD or RVAT starters, that means that the "overcapacity" in generators (see Section 2.2) is not needed for motor starting requirements. As such, Carollo's recommendation is that the County not use Generator 3, by either: 1) abandoning it in place, "winterizing" it until a generator is needed elsewhere in the County; 2) keeping it in-service as a standby unit that is not paralleled with Generators 1 & 2 (but still connected to the SWGR-GEN); or 3) selling it.

Carollo's design philosophy, in this regard, is to provide enough generator capacity to run the entire plant in the event of a utility failure: considered an "N" level of redundancy in standby generators. The utility service and two paralleled generators would make N+1 redundancy, and the present arrangement of utility service and three generators could be considered N+2 redundancy. Our experience has been that N+1 redundancy is most common at Florida plants and around the United States. Another factor is that MARS pumping, which represents half of the plant load, can be provided from the NEWRF or SWWRF in the unlikely event that a FP&L failure at SEWRF is coincident with a failure of one of your standby generators. An N level of redundancy is less expensive to provide, maintain, and replace than an N. The recommendations in this report develop that philosophy over the course of several projects.

3.6 Equipment Vulnerabilities: Two Assemblies of Generator Switchgear

Generators 1 &2 Switchgear (G12-SWGR) was manufactured in 1995 and Generators 2 & 3 Switchgear (G23-SWGR) was manufactured in 2001. At the time of Carollo's inspection, Generator 1 had been run for 491.3 and Generator 2 had been run for 243 hours. This translates to about 2 hours of operation per month for each generator, suggesting that the generator exercising habits mentioned in Section 3.4 are a recent aberration; that exercise has been mostly diligent for the history of the equipment.

Site visit observations found both of the Generator Switchgears to be in good condition. G12-SWGR had an active alarm for "Low Fuel Level Day Tank" on Generator 2 from the last time, a month previous, when the generator ran, and that it shut down the generator. This raises the questions: why is the alarm light still on, is there any remote notification, and how does fuel get ordered? A month should be plenty of time to address low fuel level. A push test on the G12-SWGR annunciator also found that the "Generator 2 CB Open" light is out and the "Control Voltage Failure" (for Unit 1) light is out. The standby power system should be considered a critical system with a high priority level for maintenance; any issues concerning the standby power system should be immediately addressed.

Looking only the age and condition of G12-SWGR and G23-SWGR, the equipment is suitable for a full 30 years of service. Unfortunately, their functionality is not well-matched to the present demands of the plant. Specifically, neither G12-SWGR nor G23-SWGR is able to synchronize its generators together to operate in parallel; so none of the generators are able to share duties for powering the plant. This is because the switchgear bus of Generator 1 is not physically attached to the switchgear bus of Generator 2 inside the G12-SWGR assembly (obviously, paralleling controls are absent as well). The same is true of the G23-SWGR. Instead of paralleling the generators, Generator 1 is dedicated to the A-bus of SWGR-1A/B and Generator 3 is dedicated to the B-bus of SWGR-2A/B. In both cases, a single generator could supply power to both buses of its own assembly if the tie circuit breaker is open, but neither can share the load duties with another generator. In total, the plant has four independent switchgear buses in two switchgear assemblies receive power from three standby generators. It's a confusing arrangement that's difficult for staff to use effectively. In addition, it requires over-investment in generators to make enough power available to back up all processes.

Considering the observations just described, the required replacement of SWGR-1A/B, and the benefits of improving distribution of the SEWRF's standby generators, Carollo recommends replacing this equipment early, at the same time as SWGR-1A/B. These two assemblies (G12-SWGR and G23-SWGR) should be replaced with one assembly, instead of two, that is capable of paralleling Generators 1 & 2. That paralleling generator switchgear will be referred to as SWGR-GEN in this report. The County may wish to keep Generator 3 available for non-paralleling duty - and possibly a load bank for exercising it - in which case another two circuit breakers might be needed in SWGR-GEN, but the primary purpose for the switchgear is to parallel Generator 1 and Generator 2 for distribution to the plant.

The reason that Generator 3 is difficult to parallel to the other two is the pitch of the generator windings. The two units from 1995 have pitches of 0.7619, and the generator from 2001 has a pitch of 0.6667. Ideally, paralleling is most easily achieved between generators whose pitch matches, so it's more complicated to parallel the 2001 unit with the two others. It is possible for generators with mismatched pitches to be paralleled, but Ring Power has had bad experience with the multiple winding reactors - and a 3rd generator is probably not needed (because of good utility power, N+1 redundancy, and the ability to serve MARS loads from elsewhere).

Carollo recommends that the County provide paralleling switchgear (SWGR-GEN) when replacing SWGR-1A/B, and making a connection to the service switchgear (SWGR-1A/T/B) at a transfer bus between two tie circuit breakers. (see drawing EMP-2019). Although this is ahead of schedule for the typical 30-year replacement cycle, it would be more operationally flexible, easier to use, as reliable, and less expensive (long term) than the current configuration.

3.7 Equipment Vulnerabilities: Original Motor Control Centers

Built in 1986, MCCs -5 and -6 are past their expected 30-year service life, especially considering the humid environment in which they operate. In equipment this old the insulation deteriorates, creating the potential for short circuits and arc flash incidents, the reliability of the overcurrent protection degrades as factory-lubricated mechanisms dry out over time, and repairs can be longer and more costly when spare parts aren't available. These motor control centers are critical to the operation of the solids processing performed by the SEWRF's belt filter presses, and their age and poor condition compromises reliability.

The situation for MCC-9 and MCC-10 is similar to that of MCCs -5 and -6: both are 30 years old, past their expected service life. In addition, these MCCs have an inadequate short circuit rating for the application, and they've had instances when circuit breakers failed to open on short circuit faults. They're closely linked, as well: MCC-9 (which was probably originally labeled MCC-3) is the power source for MCC-5 and MCC-10 (originally labeled MCC-4) is the source for MCC-6. All four MCCs are functional and safety liabilities, and they all should be replaced as soon as possible.

In 2018 the RAS/WAS rehabilitation project will replace the existing scum ejectors and air compressors with progressive cavity pumps, one pump (~10 HP) for each secondary clarifier, requiring four size-1 starters. Although these would ideally be supplied from MCC-11 and MCC-12 (which are in the Main Electrical Room) to match the clarifiers and RAS/WAS pumps, bucket space is not available there, and MCC-11 doesn't have room to add another vertical section. There is an existing FVNR starter for each scum ejector in MCC-10, implying that there is an underground conduit path from MCC-9 and MCC-10 to the RAS/WAS pumping area, which could be re-purposed for the new pumps.

Carollo recommends replacing MCC-9 and MCC-10 in the RAS/WAS rehabilitation project, and the replacement VFDs for the RAS and WAS pumps should be included in the replacement MCCs -9 and -10 (rather than having the units separately-mounted in the Main Electrical Room, as they are now) to provide the cleanest installation. This option would be less expensive than

having them separately mounted, and the County could still connect to the existing conduit by a conduit extension to the new motor control center. This option, which would be less expensive than replacing the existing separately-mounted VFDs, is not reflected in the costs shown in Project Recommendations.

The outgoing feeder circuits from MCCs -9 & -10 to MCCs -5 & -6 should be extended to an upstream switchgear source: SWGR-2A/B, preferably. The placement of replacement MCCs -9 & -10 should take into account the conduit penetrations for the feeders to MCC-5 and MCC-6, so that they can be extended to a switchgear source without passing through the motor control center.

3.8 Equipment Vulnerabilities: Repair the MCCs Manufactured in 2000

Eight of the SEWRF's motor control centers were manufactured in 2000: MCCs -1, -2, -3, -4, -7, -8, -11, and -12. All are installed in a clean environment and in good condition. They all have digital metering and are operating within their ratings. They were installed as twin-pairs, with tie circuit breakers between MCCs -1&2, -3&4, -7&8, and -11&12. MCCs – 1&2 and 3&4 power the Aerators, Anoxic Mixers, RML Pumps, and EQ Pumps; MCC-7&8 power the Sludge Thickening Pumps; MCC - 11&12 power the Clarifier Drives, RAS/WAS Pumps, and Lake Gravity Filters. Together, those motor control centers are the branch circuit source for nearly all of the SEWRF water treatment processes, and as such they are critical to system reliability.

A common problem among these MCCs was low power factor, an indicator that the correction capacitors (PFCC), which are installed on the larger FVNR starters, have failed. This is also shown on the PFCC indicator lights. Carollo recommends replacing the PFCCs. MCCs -11 and - 12 both have very low power factor and high harmonic current distortion: this should be investigated. The current distortion could be mitigated with input filters on the VFDs for the RAS/WAS Pumps, and a PFCC on the RVAT for the Air Scour Blower might fix the power factor. Alternatively, an active harmonic filter could solve both problems.

Considering the criticality of these MCCs (1, 2, 3, 4, 7, 8, 11, & 12) for another 12 years, Carollo recommends maintaining spare parts for these units, especially for the RVAT starters for the Sludge Blowers, which were being repaired on several visits. Other minor problems are mentioned below under Short Term Improvements, and won't be repeated here.

3.9 Equipment Vulnerabilities: Replace the Original Panelboards

The panelboards and transfer switches manufactured from 1986-1989 should be replaced as part of the capital improvement projects that have already been listed. The remaining panelboards - those installed after 1988 - can be replaced on a typical 30-year schedule. Refer to the SEWRF Equipment Condition Assessment table for years of each panelboard.

3.10 Equipment Vulnerabilities: Plan to replace VFDs at 20-year intervals

Variable frequency drives (VFD) can have a service life from 9 years to over 20 years, depending on the duty to which they're subjected and the environment in which they're installed.

Just as the corrosion of metals and deterioration of insulation happens to circuit breakers, VFDs have the additional problem of high frequency electrical switching that's required for the technology to chop up a sine wave of electricity and reconstruct it as an approximation of a sine wave. Considering that the SEWRF applications have clean environments without severe torque requirements or overloads, Carollo recommends that the SEWRF plans to replace their VFDs at 20-year intervals.

4.0 PROPOSED RECONFIGURATION OF ELECTRICAL SYSTEM

With three generators connected through four independent circuit breakers in two different switchgear line-ups, to four buses of service switchgear, the SEWRF's power system architecture is not intuitive - making it inherently confusing to operate and maintain. The theme of these proposals is consolidation and centralization: consolidating two service entrance switchgears into one; and consolidating two generator switchgears into one.

4.1 One Service Entrance Switchgear with Three Buses

Due to the age and condition of the existing SWGR-1A/T/B, as described in the condition assessment, a new service entrance switchgear, SWGR-1A/T/B, is proposed to replace SWGR-1A/B in the same location (the bulk of the plant can already by powered by SWGR-2A/B). As shown on EMP-2019, the new switchgear will be configured as the single point of connection for power from both FP&L transformers and for the standby generators. In the new arrangement, each FP&L transformer supplies one bus of SWGR-1A/T/B. Standby power connects between the tie breakers from a new Generator Switchgear (SWGR-GEN, see below). Co-Generation would remain connected at SWGR-2A. SWGR-2A/B will be fed from SWGR-1A/T/B rather than service circuits from FP&L transformers. All feeder circuits from SWGR-1A/T/B and existing SWGR-2A/B will remain as currently connected.

The new arrangement enables all plant loads to any load in the plant access to FP&L1, FP&L2, and SWGR-GEN through use of the tie breakers. Also, an outage (planned or unplanned) on any of the four switchgear buses would still provide the remaining buses access to all of its generating capacity. Similarly, an outage to any bus except SWGR-2A would retain access to Co-Gen power for the remaining two buses through the use of the tie breakers. Further, by being downstream from the service entrances, SWGR-2A/B could take outages without having energized conductors on the line side of the main breakers. A system that is convenient to take outages and intuitive to operate is safer, more reliable, and more available. Also, with the plant utilizing three different power sources (utility, co-gen, and standby), the network will be better-suited to distribute all three sources from a single switchgear assembly that still retains alternate circuit paths in the form of multiple buses and redundant feeders.

4.2 One Generator Switchgear to Parallel 2 Generators (with or without 3)

One-line drawing EMP-2018 details the current configuration where the three generators are connected to four circuit breakers in two separate generator switchgear assemblies. One-line diagram, EMP-2019, details a new generator switchgear, SWGR-GEN, that parallels all three units on a single bus. As discussed above in the Condition Assessment, the SEWRF could probably be run from two generators if they were "paralleled" to share loads on a common bus, but it's reasonable that the County would want to keep a spare standby generator and then would keep the third unit. Regardless, generator power would be much more widely available and easily dispatch-able if the units were networked in the manner described here.

The sequence of projects, dictates that the Generator system modifications occur at the same time as SWGR-1A/T/B in 2019. The 2019 switchgear replacement provides the advantage that either FP&L service would be available to the entire facility. Likewise the 2019 power system configuration makes the standby power system available to the entire facility through this service entrance switchgear. Therefore the standby power systems and service entrance switchgear projects need to be on the same timeline.

Carollo sees the biggest incentive to paralleling switchgear as the ability to eliminate the replacement cost for one generator, which would be ~\$1.5 million dollars (though that cost wouldn't be incurred for several years, since the County already owns 3 generators at this plant). Granted, the paralleling switchgear will cost several hundred thousand dollars, but it will be much less expensive than replacing the third generator. If the County has a need for 2000 kW generator elsewhere at its utility facilities, then Generator 3 could be re-purposed for that application. Otherwise it could be sold or left in-place as a stand-alone unit that can't be paralleled with the other two generators.

4.3 Removing or Replacing SWGR-2A/B in 2032

SWGR-2A/B was manufactured in 2001 and installed in 2002, so in 2032 it will be 30 years old and due for replacement. One option would be for the switchgear to be replaced with a similar unit. In this scenario, the Co-Gen connection remains downstream of the same (A) bus as the FP&L main breaker to which it is tied (any other location for it is sub-optimal). Several features of this arrangement make it attractive: 1) the feeder connections and conduit are already in place; 2) with SWGR-2A/B downstream from SWGR-1A/T/B, any three (of the four) switchgear buses can serve power to their loads; and 3) it provides the plant with a second piece of distribution equipment that loads can migrate to when SWGR-1A/T/B is eventually replaced. Considering its potential to serve as replacement when the service switchgear SWGR-1A/T/B is retired, the replacement for SWGR-2A/B could be specified to "service switchgear" standards and expanded to include a transfer bus, becoming: SWGR-2A/T/B. In this instance, SWGR-2A/T/B could receive a feeder direct from SWGR-GEN. This configuration is not shown in master plan drawings, but would be very similar to EMP-2035, but with a transfer bus between SWGR-2A and SWGR-2B.

The alternative to replacing SWGR-2A/B would be to eliminate it entirely, migrating all of its loads and Co-Gen to SWGR-1A/T/B, as shown on drawing EMP-2031. The remainder of SWGR-2 loads would be migrated to SWGR-1. The downside of this arrangement is that an outage to either bus would take out half of the plant. One benefit of this arrangement is that it would be relatively inexpensive to implement if the plant installs SWGR-1A/T/B with enough space to add five vertical sections between the two buses. Another benefit would be leaving a large space where SWGR-2A/B is currently located - accommodating the future work of replacing SWGR-1A/T/B/ with similar unit that could be installed concurrently with the existing one.

The execution of one of these options for SWGR-2 will be in 2032, but choices made during the replacement of SWGR-1A/B will impact the options that are available to the County when that

project is developed. Carollo's recommendation is to leave room for expansion when SWGR-1A/T/B is installed, but defer a commitment on SWGR-2 until a later date..

4.4 Retain Ties between Twin-Pair MCCs

With the improvements described above and the existing tie circuit breaker connections between MCCs, the SEWRF will have eliminated all single points of failure between the branch circuit protection of its MCCs and the supply circuit from all its four power sources, and it will have provided all loads in the plant with redundant paths to Co-Gen power, multiple utility transformers, and multiple sources of standby power.

4.5 New MCC and Electrical Building for Anoxic/Aeration Basin #4 in 2026

Several aeration solutions are being considered for the future fourth basin, and the electrical requirements will depend on which solution is selected. The estimate here presumes that the fourth basin will match the existing Basins 1, 2, and 3 without any return mixed liquor pumps.

The drawings indicate that existing MCC-4 was intended as the source for Aeration Basin 4. However, some of the space reserved for that basin's loads has been used for two equalization pumps and one equalization blower. MCC-4 is rated for 1200 A, and its maximum historical demand load is ~900 A. Because it is unclear whether that maximum is old or recent, all of the meters need to be reset as part of an improved data-gathering practice identified in the "Short Term Improvements" of 2019 (see Section 2.1). At this MCC in particular, resetting the meters will allow for a more accurate sense of available capacity. MCC-1 and MCC-2 appear to have more available electrical capacity, but space is a constraint for both, and it is not yet clear what electrical demand MCC-SEP will place on MCC-1.

Regardless of the available capacity of the MCC-4 bus, there is not enough room in the electrical room of the existing Aeration Basin/Headworks Building to add the starters for Basin 4. However, the replacement of all of the MCCs in that space (MCC-1, -1A, -2, -2A, -3, -4) is scheduled for 2030, and the starters for Basin 4 could be incorporated into that space if the schedule for replacement of those MCCs was moved up, from 2030 to 2026.

An alternative to locating the new loads into the existing electrical room at the Aeration Basin/Headworks Building would be to provide a new building between Basins 2 & 3 (or Basins 3 & 4) to house the distribution equipment for those areas as well as for Flow Equalization Tank 2. This option relieves space constraints in the existing electrical room at the Aeration Basin/Headworks Building; however, it does incur cost for the building, its supply circuit, and a PLC (or RTU) for that space. The costs of this a new building with motor control center, panelboards, and PLC cabinet are assumed in the cost estimate for this work (see Section 7.9).

5.0 OPERATIONAL IMPROVEMENTS

This set of recommendations has the potential to improve the safety and reliability of the SEWRF - as well as minimizing its overall cost of ownership. These recommendations also have the potential to improve the quality of future construction and to lower the overall cost of ownership for the plant.

5.1 Establish a Stricter Practice of Maintaining Plant Documentation

SEWRF record drawings aren't easily accessible. In some cases, in order to understand the power system it was necessary to refer to intermediate submittals, bid drawings, and manufacturer's drawings instead of record drawings. A number of things were missing from the available drawing sets, and errors were common between the documents and the field installation.

The electrical content of the record drawings is not well developed. Resulting in poor record of an installation, and the plant's drawings become difficult to use and maintain. These even become a safety liability, as plant staff struggle to find accurate drawings to guide their safety procedures.

- Example: 10 MG Storage Tank, sheets E-0.4 and E-0.6 indicated upstream connections for the project's new motor control centers, but provided no one-line diagrams for MCC-13 or MCC-14. All MCCs should have one-line diagrams that are updated on subsequent projects as they're modified with changes that impact the expressed information.
- Example: Biosolids Dryer, Sheet-101, provides a schedule for the loads of a new MCC, but no new one-line diagram. In addition, the motor control center re-uses a tag that's already assigned to another distribution source on plant: MCC-1. This issue is discussed below.

SEWRF will benefit if it improves its system of records management for project documentation. All of the documents should be centralized, controlled, and maintained, but still accessible and usable.

- Documents required for electrical equipment maintenance include:
 - o Installation instructions
 - o Disassembly/assembly (interconnection) drawings
 - Wiring diagrams, control schematics, and bills of materials
 - Equipment operation (for set-up and adjustment)
 - Maintenance recommendations by manufacturer (including parts list and recommended spares)
 - Software programs and troubleshooting guides (where applicable)

- Documents required for execution of your Electrical Safety Plan are:
 - One-line diagrams
 - Coordination studies
 - Training documentation
 - o Electrical Safety Plan
 - Training records for project team members

The County should use explicit language in design contracts, if it's not in there already, for Consultants to provide completed one-line diagrams for each new switchgear or MCC, and update the drawings of the equipment that is modified by their designs. Further, Contractors should be required to provide a Record Set of drawings that shows the final installation, including any deviations between the design drawings and the field work. If requirements for these services are already in Manatee County contracts, then the language should be enforced. Accurate record drawings are a requirement of NFPA 70E, the *Standard for Electrical Safety in the Workplace*.

5.2 Create a Tagging System that Uniquely Matches Labeling to Drawings

Field investigation found inconsistent use of tagging throughout the SEWRF plant. Some equipment is not tagged at all, redundant tags exist for distribution equipment, and there appear to be mismatches between drawings and load equipment. This inconsistency results in confusion by plant staff, design consultants, and contractors who work with this equipment and poses a definite safety concern. Accurate and consistent tagging is a requirement of NFPA 70E, the *Standard for Electrical Safety in the Workplace*.

The Utility should create and implement a utility-wide, standardized tagging system that can be provided to consultants and contractors for future work. A preliminary tagging standard for the SEWRF, and its application to the plant's equipment, were provided by Carollo; and a copy of the recommendations can be found in Appendixes E and F.

5.3 Define Plant Technical Standards and Preferences for Project Specs

Plant staff, expressed frustrations about their inability to control which equipment is provided for projects. They want to be able to eliminate some manufacturer's products while still maintaining competitive bids. They also want to standardize on communication protocols, instrumentation technology, and control system platforms that would enable them to limit the number of skillsets that their technicians are expected to work with.

Appendixes G, H, I, J, and K contain a sample set of Design Guidelines for this purpose, which is simply a series of lists of different types equipment, providing a template to define Owner preferences and present them to their consultants. Providing Design Guidelines to consultants will help with standardization and reduce the amount of disparate systems with the plants.

Carollo also has a few equipment-specific recommendations for all switchgear, switchboards, and motor control centers.

- Have the equipment manufacturer provide factory-installed voltage testing stations. This
 device facilitates the testing process that electricians use to verify the absence of voltage
 on distribution equipment. Having it eliminates several inconveniences of taking outages
 and can simplify your safety procedures.
- Where possible, eliminate Main Circuit Breakers downstream of the service entrance Main. This forces electricians to open the upstream feeder circuit breaker when taking outages for maintenance, construction, and repairs. When providing Main Circuit Breakers, provide Arc Reduction Mode (ARM) switches. When working on energized equipment, an electrician can us ARM switches to reduce the duration (and hence severity) of a blast, if one does occur.
- Carollo does not currently have a recommendation on the "arc-resistant construction" feature of this distribution equipment. Arc-resistant MCCs are built like a tank to contain a blast and have other features that channel blast energy out the top of the assembly and keep blast energy from travelling through neighboring compartments and vertical sections and compartments, if one does occur. The County can judge the costs and benefits on their merits.
- Supplying non-continuous and non-process loads such as overhead doors, weir operators, and valve actuators from service entrance switchgear and motor controls centers is an expensive way to serve un-critical loads. Carollo recommends serving those devices from a panelboard, instead.

5.4 Implement the Electrical Safety Plan that Carollo provided in 2017

The OSHA General Duty clause essentially requires the OWNER to provide a safe work environment. The OSHA Standards incorporate NFPA 70 (the National Electrical Code) by reference, which in turn incorporates NFPA 70E. Therefore the requirements of NFPA 70E are used to provide specifics that must be met to comply with OSHA. NFPA 70E requires, among many other things, that the OWNER provide its staff with an ESP. SEWRF's current practices do not appear to comply with the ESP, and in fact the ESP was not in use during the time of the field investigations. Therefore SEWRF's current practices do not appear to be compliant with the OSHA requirements.

In a previous project, Carollo was contracted to evaluate and review an Electrical Safety Plan that another consultant had provided to the County for its use. That investigation found several problems with the document, and Carollo provided another Electrical Safety Plan (ESP) for the County's use. The document was written to the 2015 version of NFPA 70E (*Standard for Electrical Safety in the Workplace*), which was the prevailing standard at the time. The NFPA standard has advanced to a 2018 version, but the ESP is still worth implementing if the County

is not ready yet to invest in developing an ESP to the 2018 standard. Regardless, OSHA requires updating your ESP every 3 years, so that update should be done by 2020.

5.5 Align the Electrical Preventive Maintenance program to NFPA 70B

After observing issues with SEWRF documentation, tagging, and generator maintenance, MCU may want to establish an Asset Management (AM) program or at least an Electrical Preventive Maintenance Program (EPM) based on NFPA 70B: *Recommended Practice of Electrical Equipment Maintenance*. This recommended practice or AM program can be used protect MCU's investment in their facilities by establishing a formal program to shift expenditures from expensive capital projects to less-expensive maintenance tasks,. NFPA 70E includes a requirement that employers integrate "consideration of conditions of maintenance" into their electrical safety plan, and addressing that requirement with a formal EMP based on the recommendations of NFPA 70B would then comply with the requirements of NFPA 70E and OSHA.

5.6 Record Power Meter Data Annually and Reset Meter Fields

Power meters are important instruments for monitoring the performance of an industrial process and the suitability and capacity of distribution equipment. This historical data is critical to determining the available capacity when adding loads to buses, protective equipment, and feeder circuits Power quality data such as power factor and harmonic distortion of currents and voltages, is also important is assessing the impact of additions to the power system. For the power demand, consumption, and power quality data to be used for assessing the capacity of a power system it must be historized as required by Article 220.88 (1) of the National Electrical Code.

As a minimum SEWRF should transfer or record power demand data, that is time and date stamped from all power meters on the switchgear and MCCs on a monthly basis. Once the data is gathered, the plant should reset the demand register of the meters. Historical maximums after the reset will then provide a basic power demand profile. This information provides SEWRF's operators, managers, engineers, and consultants with better data of recent and historical operating conditions. SEWRF's equipment installed before 2000 do not have digital, historical meters, but most of the more recent MCCs do (MCCs -1A and -2A do not, and the recently installed MCCs -1B and -2B have not been verified). Where possible the power demand, power factor, and harmonic information should be automatically input into the plant SCADA system, and thereby create a database of electrical power information. As new electrical equipment is added and existing equipment replaced this equipment should be specified with metering that is linked into the plant SCADA system and historized; thereby eliminating the need for staff to manually perform this task.

5.7 Establish a Procedure for taking an Annual Energy Baseline

Energy performance for a wastewater treatment plant, the energy consumed to treat a unit of raw water influent, is a valuable metric for monitoring the effectiveness of a treatment

processes. Trends in energy consumption provide insight into the impact of project and provide guidance in evaluating capital investments. The process of evaluating energy performance begins with establishing an energy baseline, and that baseline requires data.

Carollo has begun the work of establishing an energy baseline for the plant by using a spreadsheet tool, developed for this purpose by the U.S. Environmental Protection Agency, called the Energy Usage Assessment Tool (EUAT). Five years of data from electricity bills, as well as the monthly treated volumes during this time, have been entered as a start at creating a baseline for the plant. Carollo can provide the County with this spreadsheet (a file developed in MS Excel) for its use in the future, but at the time of writing, this effort is incomplete. The remaining data fields required to establish the energy baseline are the operating hours per year of the plant's major equipment, in addition to the average motor current when the loads run. The operating hours is data that can either be mined from the SCADA system historian server or estimated by plant operators. Average motor current will have to be measured manually while the load runs, until the plant acquires Smart MCCs that automatically collect this data.

Carollo recommends that the County develop a procedure for collecting average motor operating current and operating hours per year for all continuous process equipment. This could be facilitated by investing in a recording power meter that is available as a hand tool with clamp on CTs (current transformers), which are typically less than ~ \$4000; however, MCU will need to establish and enforce an ESP and provide the proper Personal Protective Equipment (PPE) in order to accomplish this task in accordance with NFPA 70E. Then, using the EPA's EUAT, the MCU can establish 2018 as a "baseline year" for energy consumption. This tool then allows staff to assess the energy performance of future process improvements and observe trends in plantwide energy consumption not seen in utility bills, process instrumentation, or live SCADA data.

6.0 SHORT TERM IMPROVEMENTS

The following short-term improvements are necessary to assess equipment functionality and identify other concerns that may not have been identified during the current study.

6.1 General Maintenance Tasks to Secure Basic Equipment Functionality

Repair or replace failed indicator lights and annunciator lights on all four switchgear assemblies.

Repair or replace failed power meter on SWGR-2B (a replacement part has been ordered at the time of writing).

Staff reported problems with circuit breakers failing to operate at the SEWRF. The recommended short term action is to exercise the breakers by opening and closing them. Further, the SEWRF should inspect and test all of its circuit breakers in accordance with ANSI/NETA Maintenance Testing Standards and correct any issues that are found. Prioritize power circuits breakers and large molded case circuit breakers (50 A and above) over small molded case circuit breakers (less than 50 A). Maintenance of motor circuit protectors should be performed with preventive maintenance on motor control equipment.

Replace the remaining power conductors to basin loads from the original construction: Aerator 1A, Aerator 1B, Aerator 1C, Aerator 2C, Anoxic Mixer 1A, Anoxic Mixer 1B, Anoxic Mixer 2A, and Anoxic Mixer 2B. Branch circuits from MCC-2 to Aerator 2A and 2B have already failed, and classified locations like an aeration basin are known to be hazardous and corrosive.

Perform a Megger test on the insulation of 30-year-old underground cables, with feeder circuits and critical equipment at the highest priority for testing. Carollo has found underground cable to be a common source of failure at wastewater treatment plants, particularly where flooding and lightning are common.

Where motor circuit protectors (MCP) are used to protect feeder circuits, replace the MCPs with molded case circuit breakers (MCCB). This installation method was used in several instances for feeder circuits to VFDs installed external to their MCC source. It's a violation of the National Electrical Code (NEC) Article 430.52 and should be corrected.

6.2 Studies and Maintenance to Remedy Power Quality Problems

Perform a harmonic study in accordance with ANSI/NETA MTS Section 6.6 and ANSI/IEEE Standard 399. Plant staff reported random circuit breaker trips throughout the system, suggesting sporadic instances of high heat at the overcurrent protective devices. This is typical of high line currents caused by a low power factor, which was observed at all motor control centers, and high harmonic currents, which was observed at MCC-11 and MCC-12.

Inspect and test the plant's grounding systems in accordance with ANSI/NETA MTS Section 7.13 and all surge arrestors in accordance with ANSI/NETA MTS Section 7.19. This recommendation is to account for corrosion problems endemic to coastal environments like

Manatee County, the high incidence of lightning strikes, the frequency of utility outages, and the observed power harmonic problems at the facility.

Replace or install power factor correction capacitors (PFCC) or line reactors for the following equipment:

- In all cases, confirm that contactors are working correctly to avoid making harmonic issues worse. PFCCs should not be left on-line when the motor with which they are associated is off-line.
- PFCCs for the nine 125 HP aerators and two 125 HP sludge blowers that are supplied by MCCs 1, 2, 3, and 4.
- PFCCs for the starters of the three 250 HP sludge blowers supplied by MCCs 7 and 8.
- Line reactors for VFDs to the 75 HP RAS Pumps and 7.5 HP WAS Pumps that are supplied by MCCs 11 and 12.
- Line reactors for VFDs to the 10 HP Sludge Feed Pumps and Gravity Belt Discharge Pumps that are supplied by MCCs 7 and 8.

Tabl	Table 6.1 Probable Construction Cost - Short Term Improvements in 2019						
No.	Description	Total					
1	Replace MCPs with MCCBs	\$8,000					
2	Replace branch circuits to four aerators & four anoxic mixers	\$10,000					
3	Replace power meter on SWGR-2B (in-progress)						
3	Provide power meter on each new MCC	see MCC replacements 2019					
4	Maintenance testing of ground system, underground cable, and harmonic study	\$20,000					
5	Protection study	\$15,000					
6	Replace power factor correction capacitors	\$40,000					
7	Provide line reactors for VFDs on RAS & WAS Pumps.	see RAS/WAS Rehab 2018					
8	Provide line reactors for VFDs on Sludge Feed and Gravity Belt Discharge Pumps.	see Arc Flash Mitigation 2019					
9	Provide line reactors for VFD-305, VFD-307, and VFD-308.	\$6,000					
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$99,000					
	Contingency (50%)	\$49,500					
Subtotal \$148,500							
	Sales Tax (7%)	\$10,395					
	TOTAL PROJECT COST ^{(3)(4) (5)} \$159,000						
Notes:							
(1) lr	(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).						

- (2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.
- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.
7.0 RECOMMENDED ELECTRICAL PROJECTS (W/ COST ESTIMATE)

The projects described in this summary are for Capital Improvement Projects (CIPs) of the electrical distribution system - as well as significant additions of electrical equipment as a part of process projects. They are organized so that installation work is grouped together where possible to reduce management, administrative costs, and disruptions to operations; however, in some instances, work that could be performed concurrently is split into two or more projects to provide flexibility to the County as it prioritizes its expenditures. The 'opinions of probable construction cost' may be used in budget projections, and the project descriptions can be used to scope Requests For Proposals (RFPs) from design consultants.

7.1 Replacements with RAS/WAS System Rehabilitation in 2018

The following list details projects recommended to take place in 2018:

- Replace the VFDs for all three RAS pumps and four WAS pumps with the "RAS and WAS System Rehabilitation" project. VFDs typically last 9-20 years, and these were installed in 2000. For VFDs larger than 50 HP, use 18-pulse technology to mitigate potential damage from voltage surges upstream and prevent power quality problems at MCC-11 and MCC-12.. For VFDs less than or equal to 50 HP, use 6-pulse technology, and potentially active harmonic filters depending on the ratio of large to small VFDs and the available short circuit current at the source. With the long distance from VFD to the RAS and WAS pumps (~600 feet), load reactors or similar filtering on the output side of the VFD should be provided. Carollo recommends contacting the manufacturer to determine what mitigation techniques need to be used in order to address dv/dt and reflect wave problems on these load circuits. When the existing cables are replaced, Carollo recommends providing shielded VFD cables to protect against high carrier frequencies and the potential for corona discharge.
- Replace MCC-9 and MCC-10. Both are 30 years old, have an inadequate short circuit rating for the application, and have had instances when circuit breakers failed to open on short circuits.
- Evaluation of the control system is outside the scope of the EMP however consideration should be given to replacing the SCADA Panel SP-1, which serves MCC-9, MCC-10, and all other motor control centers in the electrical building. SP-1 uses Rockwell Automation's SLC 5/05 line PLCs. The SLC5/05 is a discontinued and unsupported platform that is no longer manufactured, does not receive firmware updates, is becoming difficult to replace when failures occur, and is vulnerable to IT security invasions. By replacing SP-1 at the same time as the MCCs, SEWRF will pay for PLC programming only once. If they are done as separate projects, SEWRF would pay twice for PLC programming. If SEWRF selects smart MCCs (as Carollo recommends), then the cost of adding the new technology could be reduced or eliminated because smart MCCs use networked I/O rather than hard-wired I/O, avoiding installing and terminating hundreds of

wires between both enclosures. The cost does not include the reprogramming costs need for the new PLC platform.

- Replace the panelboards and transfer switches built between 1988 and 1989 and fed from MCCs 9 and 10. (MTS #3, Panel P1, MTS #4, Panel LE, Sub-Panel LE, Panel PFC, Panel LFC, Panel PC/TC-1.)
- Remove Flocculator 1 Panel, Flocculator 2 Panel, and Flocculator Control Panel, they are no longer used and in general any equipment that is no longer in-use should be demolished.

Tabl	Table 7.1 Probable Construction Cost - Replace VFDs for RAS/WAS Pumps in 2018		
No.	Description	Total	
1	Three new "engineered drive package" in separately-mounted NEMA 1 enclosure for RAS Pumps (480V, 75 HP, 18-pulse)	\$135,000	
2	Three new "engineered drive package" in separately-mounted NEMA 1 enclosure for WAS Pumps (480V, 6-pulse, 7.5 HP, line reactor, load reactor)	\$60,000	
3	Demo 12 vertical sections from 4 MCCs	\$5,000	
4	Replace with 6 vertical sections in 2 smart MCCs	\$105,000	
5	Replace SP-1 with a new PCM (CompactLogix PLC system, 6 cards of I/O, network connections to MCC). Programming cost not included.	\$100,000	
6	Replace 2 manual transfer switches (150A), and 6 panelboards (150A).	\$40,000	
6	Wiring and conduits	\$30,000	
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$475,000	
	Contingency (50%)	\$237,500	
	Subtotal	\$712,500	
	Sales Tax (7%)	\$49,875	
	TOTAL PROJECT COST ^{(3)(4) (5)}	\$763,000	

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

(5) Class 5 estimate with 50% contingency.

7.2 Dedicated Plant Drain Station in 2018

For this project, two drain stations will be added and one drain station will be improved.

The new drain station at the biosolids dryer will need a local control panel (LCP) to house the two starters for the drain station pumps, a feeder circuit, two branch circuits from LCP to pumps,

and all associated control wiring. The pumps are both assumed to be 25 HP, so the starters will be size 2 FVNR, and the conductors will be sized to match the load. The LCP will be fed from a feeder circuit breaker in MCC-1BSD in the biosolids dryer building, and the LCP will be controlled by the PLC cabinet.

The new lift station at the septage receiving facilities is assumed to have one 10 HP pump, an LCP with a size 1 FVNR, power conductors for the branch and feeder circuits (sourced from MCC-SEP), and control conductors back to the septage receiving station PLC. This facility might qualify as a Classified Area by NFPA 820 - and if so the appropriate design requirements will have to be addressed.

The existing South Plant Drain Pump Station will be upgraded with three new 40-HP pumps replacing the three existing 25-HP pumps. A new LCP (three size 3 FVNR starters) will replace the existing LCP. The existing feeder circuit breaker at MCC-12 will be upgraded. Power and control conductors will be replaced.

Tabl	Table 7.2 Probable Construction Cost - Dedicated Plant Drain Station in 2018			
No.	Description	Total		
1	Duplex local control panel with size 2 FVNR starters and integral disconnect in NEMA 4X enclosure.	\$20,000		
2	Feeder circuit: 100' of 3#4(PH) & 1#6(G) in a 2" PVC-80	\$3,000		
3	Branch circuits: 40' of 3#8(PH) & 1#8(G) in a 3/4" GRC	\$1,500		
4	Local control panel with one size 1 FVNR starter and integral disconnect in NEMA 4X enclosure.	\$2,000		
5	Feeder & branch circuits: 50' of 3#10(PH) & 1#10(G) in a 2" PVC-80	\$1,000		
6	Replace existing triplex local control panel with new: size 3 FVNR starters and integral disconnect in NEMA 4X enclosure.	\$15,000		
7	Feeder circuit: 200' of 3#3/0(PH) & 1#3(G) in existing conduit	\$5,000		
8	Branch circuits: 60' of 3#6(PH) & 1#6(G) in existing conduit	\$2,500		
9	Miscellaneous wiring and conduits	\$5,000		
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$55,000		
	Contingency (50%)	\$27,500		
	Subtotal	\$82,500		
	Sales Tax (7%)	\$5,775		
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾⁽⁵⁾	\$89,000		
Notes) }			

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.3 Replace SWGR-1A/B and Generator Switchboards 1/2 & 2/3, in 2019

The following list details projects recommended to take place in 2019:

- Replace SWGR-1A/B with new switchgear, including new main circuit breakers with digital meters, new feeders to supply SWGR-2A/B (see drawing 03E26, Appendix L), new battery charger, and new batteries for control power.
- Replace Generators 1&2 Switchgear and Generators 2&3 Switchgear with SWGR-GEN at the same time as SWGR-1A/B. The replacement switchgear should be capable of paralleling Generator 1 and Generator 2 and the County might wish to have Generator 3 as well, though without the ability to parallel with the other units (because of mismatched winding pitch, as mentioned above). SWGR-GEN will connect to the distribution system at the transfer bus between two tie circuit breakers in the new SWGR-1A/T/B assembly (see drawing EMP-2019).
- Rearrange the service feeders from the FP&L transformers into the plant, dedicating one FP&L transformer to each bus of SWGR-1A/B, with SWGR-2A/B receiving its supply from SWGR-1A/B rather than directly from FP&L. One option that the plant might consider is to ask FP&L for larger transformers so that one of them could carry the load of the entire plant - in case the other transformer fails. However, this option might lead FP&L to charge the plant at a different rate to recover the cost of this service.
- An unknown variable that could impact this work is the integration of the Co-Gen with the main circuit breaker of bus SWGR-2A, which must be closed for the Co-Gen system to operate (the Co-Gen system must be grid-connected). If it's necessary to migrate that connection point to SWGR-1A/T/B, then cost would be associated with that change as well. Integration of Co-Gen is outside the scope of this study.

Tabl	Table 7.3 Probable Construction Cost – Replace SWGR-1A/B, Gen Swgr in 2019		
No.	Description	Total	
1	Temporary power to keep existing process equipment in	\$30,000	
	operation		
2	Remove SWGR-1A/B (480V, 4000A)	\$4,000	
3	Remove Generators 1&2 Switchgear (480V, 4000A)	\$4,000	
4	Remove Generators 2&3 Switchgear (480V, 4000A)	\$4,000	
5	Replace with new SWGR-1A/B (480V, arc-resistant low voltage	\$510,000	
	switchgear, 4000A, 3-bus, nine vertical sections)		
6	Replace with new Generator Switchgear (480V, 4000A)	\$200,000	
7	Replace battery charger and batteries (48V, 12ADC)	\$25,000	
8	Miscellaneous wiring and conduits	\$50,000	
9	Building allowance	\$50,000	
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$877,000	
	Contingency (50%)	\$438,500	
	Subtotal	\$1,315,500	

	Sales Tax (7%)	\$92,085
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾⁽⁵⁾	\$1,408,000
Notes (1) Ir (2) M (2) M (3) C (4) F (5) C	3: Includes material, labor, general expenses, equipment, overhead (10%), and Market escalators for local labor and material are used in the cost estimating 6.6% of the national average, and labor is 64% of the national average. Does not include engineering, bonds, permit, and Owner's reserve for chang Rounded up to the next thousand. Class 5 estimate with 50% contingency.	profit (5%). program. Material is e orders.
(0) 0		

7.4 Replace MCC-5 and MCC-6 (and Arc Flash Mitigation) in 2019

The following list details projects recommended to take place in 2019:

- Replace MCC-5 and MCC-6. They're old amd missing parts.
- Replace the SCADA Panel (SP-4) because it controls MCC-5 and MCC-6. The PLC equipment in SP-4 is all Rockwell Automation's SLC 5/05 line, and the benefits of replacing it with the MCCs they serve are discussed above.
- Replace the VFDs installed in 2000 for the sludge pumps: VFD-301, VFD-302, VFD-303, VFD-304, and VFD-306. VFDs typically last 9-20 years, and these are near the end of their service life. When replacing them, provide a line reactor on the drive input to mitigate the potential damage from voltage surges upstream, and mitigate power quality problems at their sources, MCC-7 and MCC-8.
- Replace the panelboards and manual transfer switches installed between 1988 and 1989: MTS-LD, Panel LD, MTS-LHW, Panel-LHW, and Panel PC/TC.
- Install a new service entrance circuit breaker (1600 A) between the FP&L transformer and MCC-1BSD (at the biosolids dryer) to reduce fault clearing time at MCC-1BSD. This will lower the arc flash hazard on that motor control center.
- Rehabilitate the SEWRF's equipment tagging system. See Section 5.2 of Operational Improvements.
- Update safety labeling with a plant-wide arc flash evaluation. The SEWRF's last arc flash evaluation was in 2015. NFPA 70E requires that an arc flash hazard analysis be reviewed every five years or when significant changes are made to the system. Thus, the MCU should have a new arc flash evaluation under this project, put updated labels on all its equipment, and train its staff to use the equipment in accordance with its Electrical Safety Plan (ESP). Responsibilities should be assigned as recommended in the ESP and Job Hazard Analysis procedures for common tasks written in the ESP.

Tabl	e 7.4 Probable Construction Cost - Replacement of MCC 5 & I	MCC 6, 2019
No.	Description	Total
1	Demo 12 vertical sections from 4 MCCs	\$5,000
2	Demo panelboard, transfer switch, SP-4	\$4,000
3	Replace with 10 vertical sections in 2 Smart MCCs	\$177,000
4	Replace SP-4 with a new PCM (CompactLogix PLC system, 6 cards of I/O, network connections to MCC). Programming cost not included.	\$50,000
5	Five new separately-mounted VFDs in NEMA 1 enclosure for sludge pumps (480V, 6-pulse, 10 HP, line reactor and load reactor)	\$53,000
6	Replace 2 manual transfer switches (150A), 3 panelboards (150A).	\$28,000
7	New service entrance circuit breaker for MCC 1BSD (480V, 3PH, 1600A)	\$38,000
8	Update equipment tagging across the site and in one-line drawings.	\$30,000
9	Arc flash study.	\$20,000
10	Miscellaneous wiring and conduits.	\$20,000
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$425,000
	Contingency (50%)	\$212,500
	Subtotal	\$637,500
	Sales Tax (7%)	\$44,625
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾⁽⁵⁾	\$683,000
Notes	<u>s:</u> ncludes material, labor, general expenses, equipment, overhead (10%), and p	profit (5%).

Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).
 Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.5 Anoxic Basins Mixer Replacements, 2020

Carollo recommends replacing the anoxic mixers in basins 1, 2, and 3, with possible changes to the aerators, as well. Both new surface aerators and fine bubble diffusion are being considered, and the electrical requirements for installing that equipment would depend on which solution is selected. This estimate focus only on the mixers replacement already planned:

The following list details projects recommended to take place in 2020:

 Replace existing conductors, exposed conduit, and disconnect switches for aerators and mixers. Aeration basins are known for being corrosive and hazardous environments, and branch circuits to Aerator 2A and 2B have already failed at the SEWRF. The plant should replace them under this project. There is also a substantial risk that conduits that have been buried for a long time are filled with sand and not re-usable. If that is the case, then the underground conduit will have to be replaced and the cost will increase accordingly.

Tabl	Table 7.5 Probable Construction Cost - Anoxic/Aeration Upgrades, 2020		
No.	Description	Total	
1	Replace conductors in existing conduit 3200 feet of 3-#10 (PH) & 1-#10 (G) for all 6 anoxic mixers.	\$87,000	
2	Replace 6 60A, N4X disconnect switches for anoxic mixers.	\$30,000	
3	Replace conductors in existing conduit 1300 feet of 6-#3/0 (PH) & 1-#4 (G) for 4 aerators (1A, 1B, 3A, 3B).	\$56,000	
4	Replace 6 250A, N4X disconnect switches for aerators.	\$71,000	
5	Demo 4 30-HP VFDs for the RML pumps.	\$4,000	
	TOTAL DIRECT COST	\$248,000	
	Contingency (50%)	\$124,000	
	Subtotal	\$372,000	
	Sales Tax (7%)	\$26,000	
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$399,000	
Notor			

• Remove the VFDs for the RML pumps, which are also being removed.

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.6 Flow Equalization Tanks and Mixed Liquor Splitter Box Rehab in 2021

The following list details projects recommended to take place in 2021:

- Replace existing conductors and control panels for five submersible pumps.
- Upgrade existing lighting to LEDs.

Table 7.6 Probable Construction Cost - Flow Equalization Tanks Rehab, 2021		
No.	Description	Total
	Replace conductors for 2 30-HP submersible pumps in existing conduit: 400 feet of 3-#8 (PH) & 1-#8 (G).	\$8,000
	Replace conductors for 3 10-HP submersible pumps in existing conduit: 750 feet of 3-#12 (PH) & 1-#12 (G).	\$8,000
	Replace local control panel for 5 submersible pumps (HOA with Start and Stop pushbuttons).	\$3,000
	Replace existing lighting with LED. Assume 30 exterior pole- mounted lights on tanks and basins.	\$38,000
	New conductors in existing conduit for LED lights. Assume 2,000' of 3-#12 (PH) & 1-#12 (G).	\$11,000
	TOTAL DIRECT COST	\$68,000
	Contingency (25%)	\$34,000
	Subtotal	\$102,000
	Sales Tax (7%)	\$7,140
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$110,000

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.7 Replace BFP Control Panels with Belt Filter Press Upgrades, 2022

The following list details projects recommended to take place in 2022:

• Replace the existing BFP control panels, since they are all 30 years old and in terrible condition.

Tabl	Table 7.7 Probable Construction Cost - Replacement of BFP Control Panels, 2022		
No.	Description	Total	
1	Replace 3 control panels for existing belt filter presses	\$225,000	
2	Miscellaneous wiring and conduits	\$20,000	
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$245,000	
	Contingency (50%)	\$122,500	
	Subtotal	\$367,500	
	Sales Tax (7%)	\$25,725	
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$394,000	
		-	

Notes:

- (1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).
- (2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.
- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.8 Secondary Clarifiers Rehabilitation, 2022

The following list details projects recommended to take place in 2022:

- Replace the disconnect switch and control panel for Clarifiers 1 and 2. They appear to ٠ be the original equipment installed in 1989.
- Update arc flash study and labeling. •

Tabl	Table 7.8 Probable Construction Cost - Secondary Clarifiers Rehabilitation in 2022		
No.	Description	Total	
1	Demolition	\$1,000	
2	Replace 2 60A, N4X disconnect switches	\$10,000	
3	Replace 2 LCPs (separately mounted non-combo motor starters: 1 HP, FVNR1)	\$7,000	
4	Miscellaneous wiring and conduits for retrofit transitions	\$2,000	
5	Arc flash study	\$20,000	
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$40,000	
	Contingency (50%)	\$20,000	
	Subtotal	\$60,000	
	Sales Tax (7%)	\$4,200	
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$65,000	
Notes	<u>.</u>		

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.9 New MCC and Electrical Building for Anoxic/Aeration Basin #4 in 2026

The following list details the electrical portion of this project in 2026:

- 40' x 20' building with HVAC equipment.
- Eight vertical sections of new motor control center.
- One PLC cabinet.
- Two panelboards.
- New conductors and conduit in ductbank for mixers and aerators.

Tabl	Table 7.9 Probable Construction Cost - Anoxic/Aeration Basin #4 in 2026		
No.	Description	Total	
1	New electrical building with HVAC (40' x 20' @ 250 \$/sqft)	\$200,000	
2	New MCC 8 vertical sections	\$138,000	
3	New PLC cabinet	\$50,000	
4	New 2 panelboards (150 A)	\$8,000	
5	New conductors and conduit: 1200 feet of 3-#10 (PH) & 1- #10 (G) for 2 anoxic mixers.	\$33,000	
6	New 60A, N4X disconnect switches for 2 anoxic mixers	\$10,000	
7	New conductors and conduit: 700 feet of 6-#3/0 (PH) & 1-#4 (G) for 2 aerators (4A, 4B)	\$20,000	
8	New 250 A N4X disconnect switches for 2 aerators	\$24,000	
	TOTAL DIRECT COST	\$483,000	
	Contingency (50%)	\$241,500	
	Subtotal	\$724,500	
	Sales Tax (7%)	\$50,715	
TOTAL PROJECT COST(3)(4)\$776,000			
N 1 1			

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.10 Electrical System Upgrades in 2030

Many electrical components were installed in 2000, bringing them to the end of their 30-year service life in 2030 and 2031. The most significant component is SWGR-2A/B, the distribution source for nine motor control centers, one high service pump, and the connection point for the co-generation switchgear. The role of SWGR-2A/B will have changed in 2019, eliminating both its direct service connections from the FP&L transformer and its direct connections to Generators 2&3 Switchgear; it will have become a downstream distribution bus for SWGR-1A/B.

The design of the 2019 project will allocate space to accommodate the 2030 upgrades. Consolidating switchgear for Generators 1 & 2 and Generators 2 & 3 in the space that's presently occupied Generators 2&3 Switchgear (and the walking space next to it) would leave room for SWGR-1A/B to grow in either direction as it added additional vertical sections.

- The following list details projects recommended to take place in 2022:Replace MCC-1, MCC-1A, MCC-2, MCC-2A, MCC-3, MCC-4, MCC-7, MCC-8, MCC-11, and MCC-12, providing new conductors in existing conduit when possible from SWGR-1A/B. When replacing MCC-1 and MCC-2, reduce equipment, footprint, and overall cost by consolidating MCC-1 and MCC-1A into one line-up and MCC-2 and MCC- 2A into one line-up. This should include some (or all) of the space- and cost-saving measures recommended above for the project in 2026. Replacement of MCC-1, -1A, -2, -2A, -3, and -4 could be moved up to 2026, as explained above in Section 2.12.
- Replace the SCADA Panel SP-2, which serves MCC-1, MCC-1A, MCC-2, MCC-2A, MCC-3, and MCC-4. This recommendation is based on the electrical criteria discussed in this master plan - and the benefits of replacing PLC equipment at the same time as the motor control center it controls. SCADA system considerations are absent here, and a quicker replacement might be warranted based on those criteria. That is beyond the scope of this study.
- Replace the SCADA Panel SP-3 (which serves MCC-7 and MCC-8). This
 recommendation is based on the electrical criteria discussed in this master plan and the
 benefits of replacing PLC equipment at the same time as the motor control center it
 controls. SCADA system considerations are absent here, and a quicker replacement
 might be warranted based on those criteria. That is beyond the scope of this study.
- Replace the panelboards and manual transfer switches that were built between 1988 and 1989 (MTS-L1, Panel L1, Panel-P4, Panel L4, Panel LDA, Panel L2, MTS-L2, Panel L3, MTS-L3, Panel PC/TC-3). Also replace the three control panels for sludge blowers 1, 2, and 3 in the sludge building, and the disconnect switches for the air compressor and air scour blowers in the Air Scour Blower Building - and for the equalization blowers in the Headworks Electrical Building.
- Replace the co-generation circuit breaker with a new unit that connects to SWGR-1A/B. An estimate of this work is outside the scope of this project.

• Update arc flash study and labeling.

Tabl	Table 7.10 Probable Construction Cost – Electrical System Upgrades in 2030		
No.	Description	Total	
1	Add 6 new vertical sections with power circuit breakers to existing SWGR-1A/B (480V, arc-resistant low voltage switchgear, 4000A, 3-bus, 9 vertical sections)	\$150,000	
2	Demo 20 vertical sections from 4 MCCs (MCC-1, -1A, -2, -2A)	\$8,000	
3	Replace with 20 new vertical sections in 2 MCCs (MCC-1, -2)	\$344,000	
4	Demo 13 vertical sections from 2 MCCs (MCC-3, -4)	\$5,200	
5	Replace with 13 new vertical sections in 2 MCCs (MCC-3, -4)	\$223,600	
6	Demo 10 vertical sections from 2 MCCs (MCC-7, -8)	\$8,000	
7	Replace with 10 new vertical sections in MCCs (MCC-7, -8)	\$344,000	
8	Demo 9 vertical sections from 2 MCCs (MCC-11, -12)	\$3,600	
9	Replace with 9 new vertical sections in 2 MCCs (MCC-11, -12)	\$155,000	
10	Replace SP-2 with a new PCM (using a PLC platform that's appropriate for the plant and market conditions of 2035).	\$50,000	
11	Replace 7 panelboards (150A) & 3 manual transfer switches (150A),	\$60,000	
12	Replace 1 60A disconnect switch, 2 250A disconnect switches, and 3 400A disconnect switches,	\$20,000	
13	Replace 3 local control panels for sludge blowers.	\$20,000	
14	Temporary power to keep existing process equipment in operation.	\$20,000	
15	Remove SWGR-2A/B (480V, 4000A)	\$4,000	
16	Conduit and conductor to extend feeder circuits to SWGR-1A/B from the space formerly occupied by SWGR-2A/B.	\$30,000	
17	Building improvement allowance.	\$50,000	
18	Arc flash study.	\$20,000	
	TOTAL DIRECT COST	\$1,522,400	
	Contingency (50%)	\$761,200	
	Subtotal	\$2,283,600	
	Sales Tax (7%)	\$159,852	
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$2,444,000	

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.11 VFD Replacements for Sludge Pumps in 2033

The following list details projects recommended to take place in 2033:

- Replace VFDs installed in 2013 for the sludge pumps: VFD-305, VFD-307, and VFD-308. Carollo expects these last 20 years and will reach the end of service life in 2033. When replacing them, provide a line reactor on the drive input to mitigate the potential damage from voltage surges upstream and mitigate power quality problems from at their sources, MCC-7 and MCC-8.
- Update arc flash study and labeling.

Tabl	Table 7.11 Probable Construction Cost - VFD Replacements in 2033		
No.	Description	Total	
1	Three new separately-mounted VFDs in NEMA 1 enclosure for sludge pumps (480V, 6-pulse, 10 HP, line reactor, and load reactor).	\$31,000	
2	Arc flash study.	\$20,000	
3	Miscellaneous wiring and conduits.	\$5,000	
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$56,000	
	Contingency (25%)	\$28,000	
	Subtotal	\$84,000	
	Sales Tax (7%)	\$5,880	
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$90,000	
NIALA			

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

- (2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.
- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.12 MARS Equipment Replacements in 2035

The following list details projects recommended to take place in 2035:

- Replace the five 100-HP VFDs for the MARS low service pumps. When replacing these, Carollo recommends using technology that mitigates the potential damage from voltage surges upstream and power quality problems at their sources. In 2018, we typically recommend 18-pulse drives for drives above 50 HP, but the technology that's available in 2035 should dictate the solution. Cost estimates below assume 18-pulse technology.
- Replace the two 200 HP VFDs with MARS high service jockey pumps.
- Replace the four 400 HP VFDs with MARS high service pumps.
- Replace the SCADA Panel SP-6 (for the MARS system). This recommendation is based on the electrical criteria discussed in this master plan - and the benefits of replacing PLC equipment at the same time as the motor control center it controls. SCADA system considerations are absent here, and a quicker replacement might be warranted based on those criteria. That is beyond the scope of this study.
- Update arc flash study and labeling.

Tabl	Table 7.12 Probable Construction Cost - MARS Equipment Replacements in 2035								
No.	Description	Total							
1	Replace 5 separately-mounted VFDs in NEMA 1 enclosure with low service pumps (480V, 18-pulse 100 HP).	\$190,000							
2	Replace 2 separately-mounted VFDs in NEMA 1 enclosure with high service jockey pumps (480V, 18-pulse 200 HP).	\$120,000							
3	Replace 4 separately-mounted VFDs in NEMA 1 enclosure with high service jockey pumps (480V, 18-pulse 400 HP).	\$393,000							
4	Replace SP-6 with a new PCM, using a PLC platform appropriate for the plant and market conditions of 2035.	\$50,000							
5	Arc flash study.	\$20,000							
6	Miscellaneous wiring and conduits.	\$20,000							
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$793,000							
	Contingency (50%)	\$396,500							
	Subtotal	\$1,189,500							
	Sales Tax (7%)	\$83,265							
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$1,273,000							
NI-4-	•								

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.13 Replace Generator 1 in 2035

The following list details projects recommended to take place in 2035:

- Replace Generator 1, which will be 40 years old in 2035.
- Update arc flash study and labeling.

Tabl	Table 7.13 Probable Construction Cost - Replace Generator 1, 2025								
No.	Description	Total							
1	Remove existing Generator 1	\$14,000							
2	Install new Generator 1 (480V, Standby, 2000 kW, 0.8 pf)	\$1,076,000							
3	New conductors in existing conduit	\$32,000							
4	Arc flash study	\$20,000							
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$1,142,000							
	Contingency (50%)	\$571,000							
	Subtotal	\$1,713,000							
	Sales Tax (7%)	\$119,910							
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$1,833,000							
NI 1									

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.

7.14 Biosolids Equipment Replacements in 2038

The following list details projects recommended to take place in 2038:

- Replace the MCC-1BSD with integral biosolids PLC section. •
- Replace XFMR-UPS, Panel-UPS, XFMR-LIGHT, Panel LP-1.
- SP-1 will be replaced in 2018 and will be ready for replacement again in 20 years.
- SP-4 will be replaced in 2019 and will be ready for replacement again in 20 years.
- Update arc flash study and labeling. •

Tabl	Table 7.14 Probable Construction Cost - Biosolids Equipment Replacements in 2038								
No.	Description	Total							
1	Demo 15 vertical sections MCC-1BSD with integral PLC section.	\$6,000							
3	Replace with new 15 vertical section Smart MCCs with integral PLC section.	\$258,000							
5	Replace one transformer (7kVA) & two panelboards (150A).	\$10,000							
4	Replace SP-1 with a new PCM (using a PLC platform that's appropriate for the plant and market conditions of 2038).	\$50,000							
5	Arc flash study.	\$20,000							
6	Miscellaneous wiring and conduits.	\$20,000							
	TOTAL DIRECT COST(1)(2)(3)	\$367,000							
	Contingency (25%)	\$182,000							
	Subtotal	\$546,000							
	Sales Tax (7%)	\$38,220							
	TOTAL PROJECT COST	\$585,000							
Notes									

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.15 Replace Generator 2 in 2045

The following list details projects recommended to take place in 2045:

- Replace Generator 2, which will be 50 years old in 2045.
- Update arc flash study and labeling.

Tabl	Table 7.12 Probable Construction Cost - Replace Generator 2, 2033								
No.	Description	Total							
1	Remove existing Generator 2	\$14,000							
2	Install new Generator 2 (480V, Standby, 2000 kW, 0.8 pf)	\$1,076,000							
3	New conductors in existing conduit	\$32,000							
4	Arc flash study	\$20,000							
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾	\$1,142,000							
	\$571,000	\$571,000							
	Subtotal	\$1,713,000							
	\$119,910	\$83,265							
	TOTAL PROJECT COST ⁽³⁾⁽⁴⁾	\$1,833,000							

Notes:

(1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).

(2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.

(3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.

(4) Rounded up to the next thousand.

7.16 Electrical Equipment Replacements in 2045

The following list details projects recommended to take place in 2045:

- Eliminate MCC-13 and MCC-14, which house the feeder circuit breakers to externallymounted VFDs for the MARS system. No motor control is provided in either of these assemblies; they transfer these loads only to SWGR-1A/B (preferred) or one of the motor control centers that are fed by it (MCC-9, -10, -11, or -12).
- Replace Panel PC/TC-2.
- Replace MCC-SEP.
- SP-2 will be replaced in 2022 and will be ready for replacement again after 20 years.
- Update arc flash study and labeling.

Tabl	Table 7.16 Probable Construction Cost - Electrical Equipment Replacements in 2045							
No.	Description	Total						
1	Demo 6 vertical sections from 2 MCCs (MCC-13 and MCC- 14).	\$2,500						
2	Replace with 4 new vertical sections, retrofit to existing MCCs: 2 each added to MCC-9, -10.	\$65,000						
3	Demo 6 vertical sections from MCC-SEP	\$2,500						
4	Replace 1 panelboard (150A)	\$4,200						
	Replace with 6 existing sections with new MCC-SEP	\$104,000						
6	Replace SP-3 with a new PCM, using a PLC platform appropriate for the plant and market conditions of 2045.	\$50,000						
7	Arc flash study.	\$20,000						
8	Miscellaneous wiring and conduits.	\$10,000						
	TOTAL DIRECT COST ⁽¹⁾⁽²⁾⁽³⁾	\$258,200						
	Contingency (25%)	\$129,100						
	Subtotal	\$387,300						
	Sales Tax (7%)	\$27,111						
	TOTAL PROJECT COST	\$415,000						

Notes:

- (1) Includes material, labor, general expenses, equipment, overhead (10%), and profit (5%).
- (2) Market escalators for local labor and material are used in the cost estimating program. Material is 96.6% of the national average, and labor is 64% of the national average.
- (3) Does not include engineering, bonds, permit, and Owner's reserve for change orders.
- (4) Rounded up to the next thousand.
- (5) Class 5 estimate with 50% contingency.







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Manatee County Wastewater Treatment Facility Equipment Numbering Convention

Prepared by Andrew Rex (file name - EQUIP_ID.XLS)

September 16, 1997

P7 Updated: 6/9/2010 Process / Area Numbering

APPENDIX E: Area Tags & Equipment Codes

Equipment Prefix List

Process	1		The following letters will precede the Process							
Area Co	de			Area Code found to the left.						
Number	* Process Area / Type		Prefix	Equipment Type	Prefix	Equipment Type				
01	IBM Lift Station		AC(U)	AIR CONDITIONER (UNIT)	HUM	HUMIDIFIER				
11	Headworks / Septage Handling		ACF	ACTIVE COMPOST FAN	LI	LEVEL INDICATOR				
12	Primary Lift Pumping Station		ACP	AIR COMPRESSOR	LP	LIGHTING PANEL / LOCAL PANEL				
21	Primary Clarifiers		AHU	AIR HANDLING UNIT	LP	LIGHTING PANEL / LOCAL PANEL				
22	Primary Sludge Pumping Area		AI	MISC. ANALYSIS INDICATOR	LS	LIMIT SWITCH				
23	PST 4 Sludge Pumping Station		ANE	ANALYSIS EQUIP. (Detectors and Analyzers)	м	MOTOR				
24	Gravity Thickeners / Sludge Transfer Room		AV	MOTOR OPERATED DAMPER	MCC	MOTOR CONTROL CENTER				
25	Digester Complex		В	BOILER	MME	MISC. MECHANICAL EQUIPMENT				
26	Resource Recovery Complex		BF	BIOFILTER	MUA	MAKE-UP AIR UNIT				
27	Equalization Basin / Odor Treatment Complex #2		BLR	AERATION BLOWER	MXR	MIXER / AGITATOR				
28	Co-Generation Complex		BS	BAR SCREEN	PCL	PRIMARY CLARIFIER				
29	Biosolids De-watering Area		CAP	CAPACITOR	PDP	POSITIVE DISPLACEMENT PUMP (Lobe, Piston)				
30	Biosolids Cake Processing Area		CC	CONTACTOR CABINET	PFE	MISC. POLYMER FEED EQUIPMENT				
31	Secondary Pump Station		CCF	COMPOST CURING FAN	PI	PRESSURE INDICATOR				
33	Aeration Basins		CDR	CONDENSER	PNL	PANEL				
34	Blower Building		CEN	CENTRIFUGE	PP	POWER PANEL (ELECTRIC)				
35	Odor Treatment Complex #1		СР	CENTRIFUGAL PUMP	PRV	POWER ROOF VENTILATOR				
41	Interstage Pump Station (To be De-commissioned)		сv	CONTROL VALVE	PV	PRESSURE REGULATING OR RELIEF VALVE				
42	Solids Contact Tanks		CVR	CONVEYOR	PVL	PRESSURE VESSEL				
51	Secondary Clarifiers		DG	DRAIN GATE	SBR	AIR SCRUBBER				
52	Solids Contact Pump Gallery		DGE	MISC. DIGESTER GAS EQUIPMENT	SC	SPEED CONTROLLER				
53	Solids Contact MCC Room		DP	DISTRIBUTION PANEL (ELECTRIC)	SCL	SECONDARY CLARIFIER				
61	NTF Pumping Station		ES	EMERGENCY STOP SWITCH	SCR	SCREEN				
62	NTF Other Equipment		EF	EXHAUST FAN	SG	SLIDE GATE				
63	Dissolved Air Flotation Thickening Complex		F	FAN	SLG	SLUICE GATE				
71	Chlorine Storage / Feed		FAF	FOUL AIR FAN	SLP	SCREW LIFT PUMP				
72	So2 Storage / Feed		FI	FLOW INDICATOR	SP	SUMP PUMP				
73	Chlorine Contact Basin		FLT	FILTER	SPR	SPARE (Misc.)				
74	Nonpotable Water Pumping Station		GCP	GAS COMPRESSOR	sv	SOLENOID VALVE				
75	Sodium Hypochlorite (at Non-Pot building)		GDR	GRINDER	Т	MISC. TANK / BASIN				
76	UV Disinfection (Future)		GEN	GENERATOR	UH	UNIT HEATER				
81	Laboratory		н	OVERHEAD MONORAIL HOIST	v	VALVE				
82	Existing Administration Building		нх	HEAT EXCHANGER	VLP	VERTICAL LIFT PUMP				
91	Ops Center / Filter Building Upper Level	7	HE	MISC. HEADWORKS EQUIPMENT	VRV	VACUUM REGULATOR				
92	Filter Building Lower Level		HRU	HEAT RECOVERY UNIT	WI	WEIGHT INDICATOR				

* This two digit prefix will be followed by another two digits, starting at #01, and will increment by one until a series of three or more pieces of equipment are en-countered. Then the decade number will increment to the next unused series. For example, CP7401 and CP7402 would identify centrifugal pumps in the Non-pot Pumping Station. CP7411, CP7412, and CP7413 would identify three other types of centrifugal pumps there as well. Beginning with the Liquid Stream Improvements and De-watering Facility upgrades, this numbering scheme will be increased to a 5 digit number, 2 for the process area and 3 to identify equipment using the same instructions previously stated.

APPENDIX F: Area Tags & Equipment Codes EXAMPLE OF TAGGING SCHEME: THESE ARE NOT THE LOADS FROM YOUR PLANT



EQUIPMENT LIST REPORT

PROJECT INFORMATION

PROJECT CLIENT PROJECT NUMBER **REPORT BY** ANDREW REX **REPORT DATE** 5/24/2017 6:30 PM

03 MAIN	TENANCE BUI	LDING						
TAG		DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
		SHOP AIR COMPRESSOR	43_11_52	NEW	DUTY	CONSTANT SPEED	52.5	HP
		BRIDGE CRANE (TRUCK BAY)		NEW	STANDBY	CONSTANT SPEED	10.0	HP
BMS-03.900		MAINTENANCE BUILDING BMS CONTROL PANEL		NEW	DUTY		20.0	AMP
EF-03.920B		MAINTENANCE BAY EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.3	HP
	General Comments:	1,000 CFM						
EF-03.921		LOWER LEVEL STORAGE EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP
	General Comments:	2,000 CFM						
EF-03.922		TOOL STORAGE EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP
	General Comments:	1,500 CFM						
EF-03.923		OIL STORAGE EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP
	General Comments:	1,500 CFM						
EF-03.924		UPPER LEVEL STORAGE EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP
EF-03.925		JANITORIAL CLOSET EXHAUST FAN	23_34_01	NEW	DUTY		0.0	KW
	General Comments:	50 CFM						
EF-03.926		SHOWER EXHAUST FAN	23_34_01	NEW	DUTY		0.0	KW
	General Comments:	50 CFM						
EF-03.927		MEN'S RESTROOM EXHAUST FAN	23_34_01	NEW	DUTY		0.1	KW
	General Comments:	50 CFM						
EF-03.928		WOMEN'S RESTROOM EXHAUST FAN	23_34_01	NEW	DUTY		0.1	KW
	General Comments:	50 CFM						
EF-03.929		LOCKER ROOM EXHAUST FAN	23_34_01	NEW	DUTY		0.1	KW
	General Comments:	150 CFM						
EUH-03.956		OIL STORAGE ELECTRIC UNIT HEATER	23_83_01	NEW	DUTY		11.0	AMP
GUH-03.951		MAINTENANCE ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP
GUH-03.952		MAINTENANCE ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-85-01	Ν	Indoor
480	3	PB-85-02	Ν	Indoor
120	1	LP-85-02	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
120	1	LP-85-01	Ν	Indoor
480	1	PB-85-01	Ν	Indoor
120	1	LP-85-02	Ν	Indoor
120	1	LP-85-02	N	Indoor





PROJECT INFORMA	ΓΙΟΝ											
PROJEC CLIEN PROJECT NUMBE REPORT B REPORT DAT	T Image: Constraint of the second											
03 MAINTENANCE E	BUILDING											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
GUH-03.953	LOWER LEVEL STORAGE GAS UNIT HEATER	23_83_01	NEW	DUTY		1.9	AMP	120	1	LP-85-02	N	Indoor
GUH-03.954	TOOL STORAGE GAS UNIT HEATER	23_83_01	NEW	DUTY		1.9	AMP	120	1	LP-85-02	Ν	Indoor
GUH-03.955	UPPER PARTS STORAGE	23_83_01	NEW	DUTY		2.4	AMP	120	1	LP-85-02	Ν	Indoor
GWH-03.011	GAS WATER HEATER	22_42_01	NEW	DUTY		2.2	AMP	120	1	LP-85-02	Ν	Indoor
PWU-03.XXX1	SHOP PRESSURE WASHER UNIT	46_21_93	NEW	DUTY	CONSTANT SPEED	15.0	HP	480	3	PB-85-02	Ν	Indoor
TPV-03.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-85-01	Ν	Indoor
TPV-03.002	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-85-01	Ν	Indoor
General Commo	ROLLUP DOOR 03A (WEST)		NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	PB-85-02	Ν	Indoor
General Comme	ROLLUP DOOR 03B (EAST)		NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	PB-85-02	Ν	Indoor
General Comme	ents: ETAP TAG RUD-81.01											
HP-03.941	HEAT PUMP	23_81_44	NEW	DUTY		15.5	AMP	480	3	PB-85-01	Ν	Indoor
VCP-03.960	WATER PUMP FOR HEAT PUMP	23_21_23	NEW	DUTY	VARIABLE SPEED	7.4	AMP	480	3	PB-85-01	Ν	Indoor
EF-03.920A	MAINTENANCE BAY EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-85	Ν	Indoor
General Comme	ents: 9,000 CFM	00 04 04				5.0		400	2	N00.05	N	la de en
SF-03.931		23_34_01	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	N	Indoor
General Comme	ents: 3,000 CFM	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-85	N	Indoor
04 ADMIN BUILDING	3											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
ADMIN-MISC	MISCELLANEOUS LOADS IN ADMIN BUILDING		NEW	DUTY		600.0	AMP	480	3	SWB-04	Y	Indoor
10 NEW LIFT STATI	ON											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE					PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
	BRIDGE CRANE (MEZZANINE)		NEW	DUTY	CONSTANT SPEED	10.0	HP	480	3	PB-10-01	N	Indoor
	MONORAIL (PUMP ROOM)		NEW	STANDBY	CONSTANT SPEED	7.5	HP	480	3	PB-10-01	Ν	Indoor
	MONORAIL (GRADE LEVEL)		NEW	STANDBY	CONSTANT SPEED	7.5	HP	480	3	PB-10-01	Ν	Indoor
BMS-10.900	CC LIFT STATION BMS CONTROL PANEL		NEW	DUTY		20.0	AMP	120	1	LP-10-01	Ν	Indoor
EDR-10.111	SCREEN CHANNEL 1 INFLUENT GATE		NEW	DUTY		3.0	HP	480	3	PB-10-03	N	Indoor
EDR-10.119	SCREEN CHANNEL 1 EFFLUENT GATE		NEW	DUTY		3.0	HP	480	3	PB-10-03	Ν	Indoor
EDR-10.121	SCREEN CHANNEL 2 INFLUENT GATE		NEW	STANDBY		3.0	HP	480	3	PB-10-02	N	Indoor
EDR-10.129	SCREEN CHANNEL 2 EFFLUENT GATE		NEW	STANDBY		3.0	HP	480	3	PB-10-02	Ν	Indoor
EDR-10.131	SCREEN CHANNEL 3 INFLUENT GATE		NEW	STANDBY		3.0	HP	480	3	PB-10-02	N	Indoor
EDR-10.139	SCREEN CHANNEL 3 EFFLUENT GATE		NEW	STANDBY		3.0	HP	480	3	PB-10-02	Ν	Indoor

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PROJECT	INFORMATIC	N						
	PROJECT							
	CLIENT							
PR								
	REPORT BY	ANDREW REX						
	REPORT DATE	5/24/2017 6:30 PM						
10 NEW	LIFT STATION	1						
		DESCRIPTION	SPEC SECTION	STATUS	SEDVICE			
EDR-10.141		BYPASS GATE 1	SPEC SECTION	NEW	STANDBY	CONSTANT SPEED	3.0	HP
EDR-10.142		BYPASS GATE 2		NEW	STANDBY	CONSTANT SPEED	3.0	HP
EDR-10.150		WET WELL EQUALIZATION GATE		NEW	STANDBY		3.0	HP
EDR-10.211		PUMP 1 INLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.219		PUMP 1 OUTLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.221		PUMP 2 INLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.229		PUMP 2 OUTLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.231		PUMP 3 INLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.239		PUMP 3 OUTLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.241		PUMP 4 INLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.249		PUMP 4 OUTLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.251		PUMP 5 INLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.259		PUMP 5 OUTLET KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.311		EXCESS FLOW MAG METER UPSTREAM ISO KNIFE GATE		NEW	STANDBY	CONSTANT SPEED	2.0	HP
EDR-10.317		EXCESS FLOW MAG METER DOWNSTREAM ISO KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.319		EXCESS FLOW MAG METER BYPASS KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.321		HEADWORKS MAG METER UPSTREAM ISOLATION KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.327		HEADWORKS MAG METER DOWNSTREAM ISO KNIFE GATE		NEW	STANDBY		2.0	HP
EDR-10.329		HEADWORKS MAG METER BYPASS KNIFE GATE		NEW	STANDBY		2.0	HP
SF-10.933		STAIRWELL SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP
TPV-10.001		ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP
HP-10.941		CC LS HEAT PUMP 1	23_81_44	NEW	DUTY		26.5	AMP
HP-10.942		CC LS HEAT PUMP 2	23_81_44	NEW	STANDBY		26.5	AMP
EAM-10.315	General Comments	EXCESS FLOW HOLDING BASIN FCV : ETAP TAG EDR-10-01		NEW	DUTY	CONSTANT SPEED	0.5	HP
LCP-10.400		LS SUMP PUMP 1 & 2	43-25-00.10	NEW	DUTY	CONSTANT SPEED	1.5	HP
	General Comments	: ETAP TAG 10-PMP-01						
PPU-10.971		CNTRL ROOM POSITIVE PRESSURIZATION UNIT		NEW	DUTY	CONSTANT SPEED	1.5	HP
PPU-10.972		ELECT ROOM POSITIVE PRESSURIZATION UNIT		NEW	DUTY	CONSTANT SPEED	1.5	HP
VCP-10.960		WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	7.4	AMP
EF-10.921		LS EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	5.0	HP
	General Comments	: 8,800 CFM						
PMP-10.215	General Comments	LIFT STATION PUMP 1 : ETAP TAG 10A-PMP-1	43_25_13.30	NEW	DUTY	VARIABLE SPEED	110.0	HP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-03	Ν	Indoor
480	3	PB-10-03	Ν	Indoor
480	3	PB-10-03	Ν	Indoor
480	3	PB-10-03	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-03	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-02	Ν	Indoor
120	1	LP-10-01	Ν	Indoor
120	1	LP-10-01	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	Y	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	PB-10-01	N	Indoor
480	3	PB-10-01	Ν	Indoor
480	3	MCC-10B	Y	Indoor
480	3	MCC-10A	Y	Indoor

APPENDIX F: Area Tags & Equipment Codes EXAMPLE OF TAGGING SCHEME: THESE ARE NOT THE LOADS FROM YOUR PLANT



EQUIPMENT LIST REPORT

PROJECT INFORMAT	ON											
PROJECT												
CLIENT												
PROJECT NUMBER												
REPORT BY	ANDREW REX											
REPORT DATE	5/24/2017 6:30 PM											
10 NEW LIFT STATIO	N											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
PMP-10.225	LIFT STATION PUMP 2	43_25_13.30	NEW	DUTY	VARIABLE SPEED	110.0	HP	480	3	MCC-10A	Y	Indoor
General Commen	ts: ETAP TAG 10B-PMP-2											
SF-10.932	WET-WELL 2 SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-10B	Ν	Indoor
BAR-10.115	LS COARSE SCREEN 1	46_21_10	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-10A	Y	Indoor
General Commen	ts: ETAP TAG LS SCR-10-1	46 21 40		CT AND DV		2.0	חוו	490	2	MCC 10D	V	Indoor
General Commen	ts CUARSE SCREEN Z	46_21_10	FUTURE	STANDET	CONSTANT SPEED	2.0	ΠP	460	3	MCC-TOB	Ť	Indoor
BAR-10.135	LS COARSE SCREEN 3	46 21 10	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-10B	Y	Indoor
General Commen	ts: ETAP TAG LS SCR-10-2											
MAU-10.911	LS MAKEUP AIR UNIT	23_83_05	NEW	DUTY	CONSTANT SPEED	8.0	HP	480	3	PB-10-01	Y	Indoor
General Commen	ts: 8,000 CFM											
PMP-10.235	LIFT STATION PUMP 3	43_25_13.30	NEW	DUTY	VARIABLE SPEED	110.0	HP	480	3	MCC-10B	Y	Indoor
General Commen		43 25 13 30			VARIARI E SPEED	110.0	ЦD	480	3	MCC-10B	V	Indoor
General Commen	ts: FTAP TAG 10B-PMP-4	43_23_13.30		DOTT		110.0	111	400	5	MCC-TOD	I	indoor
SF-10.931	WET-WELL 1 SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-10A	N	Indoor
PMP-10.255	LIFT STATION PUMP 5	43_25_13.30	NEW	DUTY	VARIABLE SPEED	110.0	HP	480	3	MCC-10B	Y	Indoor
General Commen	ts: ETAP TAG 10A-PMP-5											
MTS-10-01	MANUAL TRANSFER SWITCH		NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-10B	Ν	Indoor
11 EXCESS FLOW H	OLDING BASIN											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EDR-11.101	CONTROL BOX GATE		NEW	DUTY	CONSTANT SPEED	3.0	HP	480	3	PB-10-03	Ν	Outdoor
20 NEW HEADWORK	S											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
BMS-20.900	HEADWORKS BMS CONTROL PANEL		NEW	DUTY		20.0	AMP	120	1	LP-20-01	N	Indoor
EDR-20.111	SCREEN INLET GATE 1		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-20-03	Y	Indoor
EDR-20.119	SCREEN OUTLET GATE 1		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-20-03	Y	Indoor
EDR-20.121	SCREEN INLET GATE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor
EDR-20.129	SCREEN OUTLET GATE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor
EDR-20.131	SCREEN INLET GATE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor
EDR-20.139	SCREEN OUTLET GATE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor
EDR-20.191	BYPASS GATE TO EFHB		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-01	Y	Indoor
EDR-20.211	GRIT INLET GATE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-03	Y	Indoor
EDR-20.221	GRIT INLET GATE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor

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PROJECT INFORMA	TION											
PROJE	ст											
CLIE	NT											
PROJECT NUMBI	ER											
REPORT I	BY ANDREW REX											
REPORT DA	TE 5/24/2017 6:30 PM											
20 NEW HEADWOR	RKS											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EDR-20.231	GRIT INLET GATE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Y	Indoor
MISC-HW	LIGHTING AND MISC. AT HEADWORKS		NEW	DUTY		25.0	KVA	208	3	LP-20-01	Y	Indoor
SF-20.931	STAIRWELL SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP	120	1	LP-20-01	Ν	Indoor
TPV-20.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-20-01	Ν	Indoor
HP-20.942	HW HEAT PUMP 2		NEW	STANDBY		15.5	AMP	480	3	PB-20-01	Ν	Indoor
PPU-20.972	HW CNTRL ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-20-01	Ν	Indoor
HP-20.941	HW HEAT PUMP 1		NEW	DUTY		15.5	AMP	480	3	PB-20-01	Ν	Indoor
VCP-20.960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	6.4	AMP	480	3	PB-20-01	Ν	Indoor
PPU-20.971	HW ELECT ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-20-01	Ν	Indoor
MTS-20-01	MANUAL TRANSFER SWITCH		NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-20B	Ν	Indoor
	ROLLUP DOOR D2002		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-20-01	Ν	Indoor
General Comm	nents: ETAP TAG RUD-81.01											
PMP-20.323	GRIT PUMP 2		FUTURE	STANDBY	CONSTANT SPEED	10.0	HP	480	3	MCC-20B	Ν	Indoor
FAN-20.892 General Comm	HW ODOR CONTROL FOUL AIR FAN 2 ments: ODOR CONTROL SCRUBBER FAN	23_34_17	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-20B	Y	Indoor
FAN-20.894	HW ODOR CONTROL FOUL AIR FAN 4	23_34_17	NEW	DUTY	CONSTANT SPEED	10.0	HP	480	3	MCC-20B	Y	Indoor
General Comm	ents: HEADWORKS ODOR CONTROL SCRUBBER FAN FOR SMA	LL SYSTEM										
MAU-20.911	HW MAKEUP AIR UNIT	23_83_05	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	PB-20-01	Y	Indoor
SWP-20.116	SCREENINGS WASHER/COMPACTOR 1	46_21_28	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-20A	Y	Indoor
SCR-20.114	FINE SCREEN 1	46_21_28	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-20A	Y	Indoor
GRD-20.411	GRIT DEWATERING UNIT 1	46_23_25	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	MCC-20A	Y	Indoor
CON-20.412	SCREW CONVEYOR 1	46_23_25	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-20A	Y	Indoor
FAN-20.891	HW ODOR CONTROL FOUL AIR FAN 1	23_34_17	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-20A	Y	Indoor
General Comm	ents: ODOR CONTROL SCRUBBER FAN											
GRD-20.421	GRIT DEWATERING UNIT 2	46_23_25	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	MCC-20B	Y	Indoor
CON-20.422	SCREW CONVEYOR 2	46_23_25	FUTURE	STANDBY	CONSTANT SPEED	1.5	HP	480	3	MCC-20B	Y	Indoor
SWP-20.136	SCREENINGS WASHER/COMPACTOR 3	46_21_28	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-20B	Y	Indoor
SCR-20.134	FINE SCREEN 3	46_21_28	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-20B	Y	Indoor
GRD-20.431	GRIT DEWATERING UNIT 3	46_23_25	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	MCC-20B	Y	Indoor
CON-20.432	SCREW CONVEYOR 3	46_23_25	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-20B	Y	Indoor
FAN-20.893	HW ODOR CONTROL FOUL AIR FAN 3	23_34_17	NEW	STANDBY	VARIABLE SPEED	40.0	HP	480	3	MCC-20A	Ν	Indoor
PMP-20.313	GRIT PUMP 1		NEW	DUTY	CONSTANT SPEED	10.0	HP	480	3	MCC-20A	Ν	Indoor
SWP-20.126	SCREENINGS WASHER/COMPACTOR 2	46_21_28	FUTURE	STANDBY	CONSTANT SPEED	5.0	HP	480	3	MCC-20B	Y	Indoor
SCR-20.124	FINE SCREEN 2	46_21_28	FUTURE	STANDBY	CONSTANT SPEED	2.0	HP	480	3	MCC-20B	Y	Indoor
PMP-20.333	GRIT PUMP 3		NEW	DUTY	CONSTANT SPEED	10.0	HP	480	3	MCC-20B	N	Indoor

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PROJECT INFORMATIO	ON											
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	5/24/2017 6:30 PM											
30 LSELECTOR BASIN												
	DESCRIPTION	SPEC SECTION	STATUS	SERVICE					DHASE		GEN DOWER	
EDR-30.110	SELECTOR BASIN MLR PLUG VALVE 1	SPEC SECTION	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-20-03	N	Indoor
EDR-30.210	SELECTOR BASIN MLR PLUG VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-03	Ν	Indoor
EDR-30.310	SELECTOR BASIN MLR PLUG VALVE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Ν	Indoor
EDR-30.410	SELECTOR BASIN MLR PLUG VALVE 4		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-20-02	Ν	Indoor
MIX-30.401	SELECTOR BASIN CHANNEL 4, MIXER 1	46 41 25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.402	SELECTOR BASIN CHANNEL 4, MIXER 2	 46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.403	SELECTOR BASIN CHANNEL 4, MIXER 3	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.404	SELECTOR BASIN CHANNEL 4, MIXER 4	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	N	Indoor
MIX-30.052	DENITRIFICATION ZONE 2 MIXER	46_41_25	NEW	DUTY	CONSTANT SPEED	8.3	HP	480	3	MCC-20B	Ν	Indoor
General Comment	s: RAS/DENITE ZONE											
MIX-30.301	SELECTOR BASIN CHANNEL 3, MIXER 1	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.302	SELECTOR BASIN CHANNEL 3, MIXER 2	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.303	SELECTOR BASIN CHANNEL 3, MIXER 3	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.304	SELECTOR BASIN CHANNEL 3, MIXER 4	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20B	Ν	Indoor
MIX-30.051	DENITRIFICATION ZONE 1 MIXER	46_41_25	NEW	DUTY	CONSTANT SPEED	8.3	HP	480	3	MCC-20A	Ν	Indoor
General Comment	s: RAS/DENITE ZONE											
MIX-30.101	SELECTOR BASIN CHANNEL 1, MIXER 1	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor
MIX-30.102	SELECTOR BASIN CHANNEL 1, MIXER 2	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	N	Indoor
MIX-30.103	SELECTOR BASIN CHANNEL 1, MIXER 3	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor
MIX-30.104	SELECTOR BASIN CHANNEL 1, MIXER 4	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	N	Indoor
MIX-30.201	SELECTOR BASIN CHANNEL 2, MIXER 1	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor
MIX-30.202	SELECTOR BASIN CHANNEL 2, MIXER 2	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor
MIX-30.203	SELECTOR BASIN CHANNEL 2, MIXER 3	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor
MIX-30.204	SELECTOR BASIN CHANNEL 2, MIXER 4	46_41_25	NEW	DUTY	CONSTANT SPEED	6.0	HP	480	3	MCC-20A	Ν	Indoor

35 | AFRATION BASINS/AB SPI ITTER BOX

JU LEVATION DAOING												
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EAM-35.105	AB1 - AIR FLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Ν	Indoor
EAM-35.205	AB2 - AIR FLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Ν	Indoor
EAM-35.305	AB3 - AIR FLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Ν	Indoor
EAM-35.405	AB4 - AIR FLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Ν	Indoor
MIX-35.111	AERATION BASIN 1, MIXER 1		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36A	Ν	Indoor
MIX-35.112	AERATION BASIN 1, MIXER 2		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36A	Ν	Indoor
MIX-35.211	AERATION BASIN 2, MIXER 1		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36A	Ν	Indoor
MIX-35.212	AERATION BASIN 2, MIXER 2		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36A	Ν	Indoor

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APPENDIX F: Area Tags & Equipment Codes EXAMPLE OF TAGGING SCHEME: THESE ARE NOT THE LOADS FROM YOUR PLANT



EQUIPMENT LIST REPORT

PROJECT INFORMATIO	ON											
PROJECT												
CLIENT												
REPORT BY	ANDREW REX											
REPORT DATE	5/24/2017 6:30 PM											
35 AFRATION BASIN	S/AB SPLITTER BOX											
TAG			STATUS	SERVICE					DUASE			
MIX-35.311	AERATION BASIN 3. MIXER 1	SPEC SECTION	NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36B	N	Indoor
General Comment	ts: ETAP TAG PMP-36.05			2011		0.0			Ū.			
MIX-35.312	AERATION BASIN 3, MIXER 2		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36B	Ν	Indoor
General Comment	ts: ETAP TAG PMP-36.06											
MIX-35.411	AERATION BASIN 4, MIXER 1		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36B	Ν	Indoor
General Comment	ts: ETAP TAG PMP-36.07											
MIX-35.412	AERATION BASIN 4, MIXER 2		NEW	DUTY	CONSTANT SPEED	3.5	HP	480	3	MCC-36B	Ν	Indoor
36 AERATION BASIN	S BLOWER BUILDING											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
	MONORAIL (BLOWER ROOM)		NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	PB-36-01	N	Indoor
ABB-MISC	MISC LOADS AT AERATION BLOWER BUILDING		NEW	DUTY		15.0	KVA	208	3	LP-36-01	Y	Indoor
ALP-96.381	WATER HEATER	22_42_01	NEW	STANDBY	CONSTANT SPEED	108.0	KW	480	3	PB-36-01	N	Indoor
BMS-36.900	AB BLOWER BUILDING BMS CONTROL PANEL		NEW	DUTY		20.0	AMP	120	1	LP-36-01	Ν	Indoor
EDR-36.112	AB BLOWER 1 DISCHARGE VALVE	40_05_64	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Y	Indoor
EDR-36.122	AB BLOWER 2 DISCHARGE VALVE	40_05_64	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Y	Indoor
EDR-36.132	AB BLOWER 3 DISCHARGE VALVE	40_05_64	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Y	Indoor
EDR-36.142	AB BLOWER 4 DISCHARGE VALVE	40_05_64	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Y	Indoor
EDR-36.152	AB BLOWER 5 DISCHARGE VALVE	40_05_64	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Y	Indoor
EDR-36.195	AERATION MAIN HEADER BLOW OFF VALVE	40_05_64	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-36-01	Ν	Indoor
FV-36.115	AB BLOWER 1 BLOW-OFF VALVE	40_05_64	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Ν	Indoor
FV-36.125	AB BLOWER 2 BLOW-OFF VALVE	40_05_64	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Ν	Indoor
FV-36.135	AB BLOWER 3 BLOW-OFF VALVE	40_05_64	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Ν	Indoor
FV-36.145	AB BLOWER 4 BLOW-OFF VALVE	40_05_64	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-02	Ν	Indoor
FV-36.155	AB BLOWER 5 BLOW-OFF VALVE	40_05_64	FUTURE	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-36-03	Ν	Indoor
GUH-36.951	BLOWER ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP	120	1	LP-36-01	Ν	Indoor
GUH-36.952	BLOWER ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP	120	1	LP-36-01	Ν	Indoor
HP-36.941	ABBB HEAT PUMP 1		NEW	DUTY		26.5	AMP	480	3	PB-36-01	Ν	Indoor
HP-36.942	ABBB HEAT PUMP 2		NEW	STANDBY		26.5	AMP	480	3	PB-36-01	Ν	Indoor
PPU-36.973	SWITCHGEAR ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-36-01	Ν	Indoor
TPV-36.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-36-01	Ν	Indoor
VCP-36.960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY		7.4	AMP	480	3	PB-36-01	Ν	Indoor
BLO-36.150	AB BLOWER 5	43_11_15	FUTURE	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-36A	Ν	Indoor
PPU-36.972	ELECT ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-36-01	Ν	Indoor
PPU-36.971	CNTRL ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-36-01	Ν	Indoor

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APPENDIX F: Area Tags & Equipment Codes EXAMPLE OF TAGGING SCHEME: THESE ARE NOT THE LOADS FROM YOUR PLANT



EQUIPMENT LIST REPORT

PROJECT IN	FORMATION											
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TROOL												
RF	EPORT DATE 5/24/2017 6:30 PM											
36 AFRATIC	ON BASINS BLOWER BUILDING											
	DESCRIPTION	SPEC SECTION	STATUS	SERVICE					PHASE		GEN POWER	
BLO-36.110	AB BLOWER 1	43 11 15	NEW	STANDBY	VARIABLE SPEED	200.0	HP	480	3	SWG-36A	N	Indoor
BLO-36.120	AB BLOWER 2	43 11 15	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-36A	Ν	Indoor
BLO-36.130	AB BLOWER 3	43 11 15	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-36B	Ν	Indoor
BLO-36.140	AB BLOWER 4	43_11_15	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-36B	Ν	Indoor
	ROLLUP DOOR 36 (SOUTH)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-36-01	Ν	Indoor
Ger	neral Comments: ETAP TAG RUD-81.01											
EF-36.921	BLOWER BLDG EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-36A	N	Indoor
Ger	neral Comments: BLOWER ROOM ROOF-MOUNTED EXHAUST FAN	00.04.04		DUTY		0.0	LID.	400	<u>^</u>	1100 000	NI	la de en
SF-36.931	BLOWER BLDG SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-36A	Ν	Indoor
MTS-36-01	MANUAL TRANSFER SWITCH		NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-36B	N	
				01741001		220.0	7 4 11	100	Ū			
40 SECOND	DARY CLARIFIERS/CLARIFIERS SPLITTER BOX											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
SC-40.110	SECONDARY CLARIFIER 1 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-45A	N	Outdoor
PMP-40.116	SC 1&2 SCUM PIT PUMP 1	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-40.117	SC 1&2 SCUM PIT PUMP 2	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-45A	Ν	Outdoor
SC-40.120	SECONDARY CLARIFIER 2 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-45A	Ν	Outdoor
SC-40.130	SECONDARY CLARIFIER 3 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-45A	N	Outdoor
PMP-40.136	SC 3&4 SCUM PIT PUMP 1	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-45A	Ν	Outdoor

TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
SC-40.110	SECONDARY CLARIFIER 1 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP
PMP-40.116	SC 1&2 SCUM PIT PUMP 1	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
PMP-40.117	SC 1&2 SCUM PIT PUMP 2	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
SC-40.120	SECONDARY CLARIFIER 2 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP
SC-40.130	SECONDARY CLARIFIER 3 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP
PMP-40.136	SC 3&4 SCUM PIT PUMP 1	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
PMP-40.137	SC 3&4 SCUM PIT PUMP 2	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
SC-40.140	SECONDARY CLARIFIER 4 DRIVE		EXISTING	DUTY	CONSTANT SPEED	1.5	HP
SC-40.150	SECONDARY CLARIFIER 5 DRIVE	46_43_24	FUTURE	DUTY	CONSTANT SPEED	1.5	HP
PMP-40.156	SC 5&6 SCUM PIT PUMP 1	43_25_13.32	FUTURE	DUTY	CONSTANT SPEED	5.0	HP
PMP-40.157	SC 5&6 SCUM PIT PUMP 2	43_25_13.32	FUTURE	DUTY	CONSTANT SPEED	5.0	HP
SC-40.160	SECONDARY CLARIFIER 6 DRIVE	46_43_24	FUTURE	DUTY	CONSTANT SPEED	1.5	HP
SC-40.170	SECONDARY CLARIFIER 7 DRIVE	46_43_24	NEW	DUTY	CONSTANT SPEED	1.5	HP
PMP-40.176	SC 7&8 SCUM PIT PUMP 1	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
PMP-40.177	SC 7&8 SCUM PIT PUMP 2	43_25_13.32	NEW	DUTY	CONSTANT SPEED	5.0	HP
SC-40.180	SECONDARY CLARIFIER 8 DRIVE	46_43_24	NEW	DUTY	CONSTANT SPEED	1.5	HP

45 RECYCLE PUMP S	TATION						
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
	RECYCLE PS BRIDGE CRANE TROLLEY	41_22_16	NEW	STANDBY	CONSTANT SPEED	1.0	HP
BMS-45.900	RPS BMS CONTROL PANEL		NEW	DUTY		20.0	AMP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45A	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor
480	3	MCC-45B	Ν	Outdoor

VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-45-01	Ν	Outdoor
120	1	LP-45-01	Ν	Outdoor





PROJECT INFORMATION	ON											
PROJECT CLIENT PROJECT NUMBER REPORT BY REPORT DATE	ANDREW REX 5/24/2017 6:30 PM											
45 RECYCLE PUMP S	TATION											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EDR-45.110	MLR PUMP 1 SUCTION PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.114	MLR PUMP 1 DISCHARGE PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.120	MLR PUMP 2 SUCTION PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.124	MLR PUMP 2 DISCHARGE PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.130	MLR PUMP 3 SUCTION PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.134	MLR PUMP 3 DISCHARGE PLUG VALVE	40_05_62	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.140	MLR PUMP 4 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.144	MLR PUMP 4 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.150	MLR PUMP 5 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.154	MLR PUMP 5 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.201	SC NO. 1 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	N	Outdoor
EDR-45.202	SC NO. 2 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.203	SC NO. 3 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.204	SC NO. 4 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.205	SC NO. 5 PLUG VALVE	40_05_62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.206	SC NO. 6 PLUG VALVE	40_05_62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.207	SC NO. 7 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.208	SC NO. 8 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.210	RAS PUMP 1 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.214	RAS PUMP 1 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.215	RAS PUMP 2 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.219	RAS PUMP 2 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.220	RAS PUMP 3 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.224	RAS PUMP 3 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.225	RAS SUCTION HEADER PUMPS 1-2 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.226	RAS SUCTION HEADER PUMPS 2-3 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.227	RAS SUCTION HEADER PUMPS 3-4 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.228	RAS SUCTION HEADER PUMPS 4-5 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.229	RAS SUCTION HEADER PUMPS 5-6 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.230	RAS PUMP 4 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.234	RAS PUMP 4 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.235	RAS PUMP 5 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.239	RAS PUMP 5 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	N	Outdoor
EDR-45.240	RAS PUMP 6 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	Ν	Outdoor
EDR-45.244	RAS PUMP 6 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-05	N	Outdoor

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PROJECT INFORMATI	ON											
PROJECT CLIENT PROJECT NUMBER REPORT BY	ANDREW REX											
			074700	0551/05				NO. 70	BULACE			
TAG EDR-45 250		40.05.62	SIAIUS	SERVICE				480	PHASE	POWER SOURCE		
EDR-45 254	RAS PUMP 7 DISCHARGE PLUG VALVE	40_05_62	NFW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	N	Outdoor
EDR-45 255	RAS PLIMP 8 SUCTION PLUG VALVE	40 05 62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.259	RAS PUMP 8 DISCHARGE PLUG VALVE	40 05 62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.260	RAS PUMP 9 SUCTION PLUG VALVE	40 05 62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.264	RAS PUMP 9 DISCHARGE PLUG VALVE	40 05 62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.265	RAS SUCTION HEADER PUMPS 7-8 PLUG VALVE	40 05 62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.266	RAS SUCTION HEADER PUMPS 8-9 PLUG VALVE	40 05 62	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.267	RAS SUCTION HEADER PUMPS 9-10 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	Ν	Outdoor
EDR-45.268	RAS SUCTION HEADER PUMPS 10-11 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.269	RAS SUCTION HEADER PUMPS 11-12 PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	Ν	Outdoor
EDR-45.270	RAS PUMP 10 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.274	RAS PUMP 10 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	Ν	Outdoor
EDR-45.275	RAS PUMP 11 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.279	RAS PUMP 11 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	Ν	Outdoor
EDR-45.280	RAS PUMP 12 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	N	Outdoor
EDR-45.284	RAS PUMP 12 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-04	Ν	Outdoor
EDR-45.300	WAS PUMP BYPASS VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-01	Ν	Outdoor
EDR-45.301	WAS SUCTION HEADER ISOLATION VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-45-01	Ν	Outdoor
EDR-45.303	WAS DISCHARGE MM ISO VALVE 1	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-01	Ν	Outdoor
EDR-45.307	WAS DISCHARGE MM ISO VALVE 2	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-01	Ν	Outdoor
EDR-45.310	WAS PUMP 1 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.314	WAS PUMP 1 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-03	Ν	Outdoor
EDR-45.320	WAS PUMP 2 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.324	WAS PUMP 2 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.330	WAS PUMP 3 SUCTION PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
EDR-45.334	WAS PUMP 3 DISCHARGE PLUG VALVE	40_05_62	NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-45-02	Ν	Outdoor
HP-45.941	RPS HEAT PUMP 1		NEW	DUTY		39.9	AMP	480	3	PB-45-01	Ν	Outdoor
TPV-45.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-45-01	Ν	Outdoor
PPU-45.971	ELECT ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-45-01	Ν	Outdoor
PMP-45.111	MLR PUMP 1	43_23_31.30	NEW	DUTY	VARIABLE SPEED	100.0	HP	480	3	SWG-45A	Ν	Outdoor
PMP-45.121	MLR PUMP 2	43_23_31.30	NEW	DUTY	VARIABLE SPEED	100.0	HP	480	3	SWG-45B	Ν	Outdoor
MTS-45-01	MANUAL TRANSFER SWITCH		NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-45B	Ν	Outdoor
VCP-45.960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	7.4	AMP	480	3	PB-45-01	Ν	Outdoor
PMP-45.131	MLR PUMP 3	43_23_31.30	NEW	DUTY	VARIABLE SPEED	100.0	HP	480	3	SWG-45A	Ν	Outdoor

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PROJECT IN	FORMATION											
	PROJECT											
	CLIENT											
PROJE												
	REPORT BY ANDREW REX											
RE	EPORT DATE 5/24/2017 6:30 PM											
45 RECYCL	E PUMP STATION											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE					PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
PMP-45.141	MLR PUMP 4	43 23 31.30	NEW	DUTY	VARIABLE SPEED	100.0	HP	480	3	SWG-45B	N	Outdoor
PMP-45.151	MLR PUMP 5	43 23 31.30	FUTURE	DUTY	VARIABLE SPEED	100.0	HP	480	3	SWG-45B	Ν	Outdoor
HP-45.942	RPS HEAT PUMP 2		NEW	STANDBY		39.9	AMP	480	3	PB-45-01	Ν	Outdoor
	RECYCLE PS BRIDGE MOTOR 2		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-45-01	Ν	Outdoor
	RECYCLE PS BRIDGE CRANE HOIST		NEW	DUTY	CONSTANT SPEED	7.5	HP	480	3	PB-45-01	Ν	Outdoor
PPU-45.972	CNTRL ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-45-01	Ν	Outdoor
EF-45.921	RPS EXHAUST FAN 1	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-45A	N	Outdoor
Gen	neral Comments: 6,000 CFM SIDEWALL MOUNTED FAN											
EF-45.923	RPS EXHAUST FAN 3	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-45A	Ν	Outdoor
Gen	neral Comments: 6,000 CFM SIDEWALL MOUNTED FAN											
MAU-45.911	RPS MAKEUP AIR UNIT	23_83_05	NEW	DUTY	CONSTANT SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
	ROLLUP DOOR 45 (EAST)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-45-01	Ν	Outdoor
Gen	neral Comments: ETAP TAG RUD-81.01											
PMP-45.211	RAS PUMP 1	43_23_31.30	NEW	DUTY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.216	RAS PUMP 2	43_23_31.30	NEW	STANDBY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.331	WAS PUMP 3	43_23_57.10	FUTURE	DUTY	VARIABLE SPEED	25.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.221	RAS PUMP 3	43_23_31.30	NEW	DUTY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.321	WAS PUMP 2	43_23_57.10	NEW	DUTY	VARIABLE SPEED	25.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.251	RAS PUMP 7	43_23_31.30	FUTURE	DUTY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.256	RAS PUMP 8	43_23_31.30	FUTURE	STANDBY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.261	RAS PUMP 9	43_23_31.30	FUTURE	DUTY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.271	RAS PUMP 10	43_23_31.30	NEW	DUTY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.276	RAS PUMP 11	43_23_31.30	NEW	STANDBY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.281	RAS PUMP 12	43_23_31.30	NEW	DUTY	VARIABLE SPEED	20.0	HP	480	3	MCC-45B	Ν	Outdoor
PMP-45.231	RAS PUMP 4	43_23_31.30	NEW	DUTY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.241	RAS PUMP 6	43_23_31.30	NEW	DUTY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.236	RAS PUMP 5	43_23_31.30	NEW	STANDBY	VARIABLE SPEED	15.0	HP	480	3	MCC-45A	Ν	Outdoor
PMP-45.311	WAS PUMP 1	43_23_57.10	NEW	DUTY	VARIABLE SPEED	25.0	HP	480	3	MCC-45A	Ν	Outdoor
EF-45.922	RPS EXHAUST FAN 2	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-45B	Ν	Outdoor
Gen	neral Comments: 6,000 CFM SIDEWALL MOUNTED FAN											
EF-45.924 Gen	RPS EXHAUST FAN 4 neral Comments: 6.000 CFM SIDEWALL MOUNTED FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-45B	Ν	Outdoor

55 FILTERS												
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
	EFFLUENT AERATION BLOWER 1		DEMO	DUTY	CONSTANT SPEED	15.0	HP	480	3	MCC-3A	Ν	Outdoor

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APPENDIX F: Area Tags & Equipment Codes EXAMPLE OF TAGGING SCHEME: THESE ARE NOT THE LOADS FROM YOUR PLANT



PROJECT

PROJECT INFORMATION

EQUIPMENT LIST REPORT

	CLIENT								
F	PROJECT NUMBER								
	REPORT BY	ANDREW REX							
	REPORT DATE	5/24/2017 6:30 PM							
55 FILT	ERS								
TAG		DESCRIPTION		SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
		EFFLUENT AERATION BLOWER 2			DEMO	DUTY	CONSTANT SPEED	15.0	HP
EDR-55.110	General Comments.	FILTER NO. 1 INLET VALVE : BUTTERFLY VALVE			EXISTING	DUTY	CONSTANT SPEED	1.0	HP
EDR-55.111	General Comments.	FILTER NO. 1 BACKWASH WASTE VA BUTTERFLY VALVE	LVE		EXISTING	DUTY	CONSTANT SPEED	1.0	HP
EDR-55.112	General Comments.	FILTER NO. 1 AIR WASH SUPPLY VA BUTTERFLY VALVE	VE		EXISTING	DUTY	CONSTANT SPEED	1.0	HP
EDR-55.120	General Comments.	FILTER NO. 2 INLET VALVE : BUTTERFLY VALVE			EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.121	General Comments.	FILTER NO. 2 BACKWASH WASTE VA BUTTERFLY VALVE	LVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.122	General Comments	FILTER NO. 2 AIR WASH SUPPLY VA	VE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.130	General Comments	FILTER NO. 3 INLET VALVE			EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.131	General Comments	FILTER NO. 3 BACKWASH WASTE VA	LVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.132		FILTER NO. 3 AIR WASH SUPPLY VA	_VE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
	General Comments.	: BUTTERFLY VALVE							
EDR-55.140	General Comments.	FILTER NO. 4 INLET VALVE : BUTTERFLY VALVE			EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.141	General Comments.	FILTER NO. 4 BACKWASH WASTE VA BUTTERFLY VALVE	LVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.142	General Comments.	FILTER NO. 4 AIR WASH SUPPLY VA BUTTERFLY VALVE	VE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.210	General Comments.	FILTER NO. 5 INLET VALVE : BUTTERFLY VALVE			EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.211	General Comments	FILTER NO. 5 BACKWASH WASTE VA	LVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.212	General Comments	FILTER NO. 5 AIR WASH SUPPLY VA	VE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.220	General Comments				EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.221	General Comments	FILTER NO. 6 BACKWASH WASTE VA	LVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.222	General Comments	FILTER NO. 6 AIR WASH SUPPLY VA	VE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP
EDR-55.230	General Comments.	FILTER NO. 7 INLET VALVE : BUTTERFLY VALVE			EXISTING	STANDBY	CONSTANT SPEED	1.0	HP

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VOLTS F	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	MCC-3B	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.100	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor
120	1	VCP-55.200	Ν	Outdoor




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	PROJECT												
P													
	REPORT BY												
	REPORT DATE	5/24/2017 6:30 PM											
55 FILTI	ERS												
TAG		DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EDR-55.231		FILTER NO. 7 BACKWASH WASTE VALVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP	120	1	VCP-55.200	Ν	Outdoor
	General Comments	: BUTTERFLY VALVE											
EDR-55.232		FILTER NO. 7 AIR WASH SUPPLY VALVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP	120	1	VCP-55.200	Ν	Outdoor
	General Comments	: BUTTERFLY VALVE											
EDR-55.240		FILTER NO. 8 INLET VALVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP	120	1	VCP-55.200	Ν	Outdoor
	General Comments	: BUTTERFLY VALVE											
EDR-55.241		FILTER NO. 8 BACKWASH WASTE VALVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP	120	1	VCP-55.200	Ν	Outdoor
	General Comments	:: BUTTERFLY VALVE											
EDR-55.242		FILTER NO. 8 AIR WASH SUPPLY VALVE		EXISTING	STANDBY	CONSTANT SPEED	1.0	HP	120	1	VCP-55.200	Ν	Outdoor
	General Comments	:: BUTTERFLY VALVE											
BLO-55.413		FILTER AIRWASH BLOWER 1		NEW	DUTY	CONSTANT SPEED	50.0	HP	480	3	MCC-60A	N	Outdoor
	General Comments	ETAP TAG BLO-60.01											
PMP-55.520		AUXILIARY BACKWASH PUMP 2		FUTURE	DUTY	CONSTANT SPEED	20.0	HP	480	3	MCC-60B	Ν	Indoor
	General Comments	ETAP TAG PMP-60-06								•			
PMP-55.510	o 10 1			EXISTING	DUTY	CONSTANT SPEED	20.0	HP	480	3	MCC-60A	N	Outdoor
	General Comments	E ETAP TAG PMP-60.01					<u> </u>	115	400	<u>^</u>		N1	0.11
EDR-55.052		F SPLITTER MOTORIZED GATE 2		FUTURE	DUTY	CONSTANT SPEED	0.5	HP	480	3	PB-60-02	N	Outdoor
	General Comments				DUTY		50.0	UD	400	2		N	Quitida en
BLU-55.423	Conorol Commente			FUTURE	DUTY	CONSTANT SPEED	50.0	HP	480	3		IN	Outdoor
EDR-55 051	General Comments	E SPLITTER MOTORIZED GATE 1		FUTURE			0.5	НР	480	3	PB-60-03	N	Outdoor
LDI1-00.001	General Comments	TTAP TAG GAT-60 01		TOTORE	DOTT	CONSTANT OF LED	0.0	111	-00	5	1 0-00-03	IN	Outdoor

60	DISINFE	ECTION	BUILDIN	G
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TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
BMS-60.900	DISINFECTION BLDG BMS CONTROL PANEL		NEW	DUTY		20.0	AMP
COS-60.010	AUTOMATIC SAMPLER	11_53_02	NEW	DUTY		0.5	HP
EDR-60.090	FILTER AUXILLIARY BACKWASH INLET GATE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EDR-60.110	UV CHANNEL 1 INFLUENT GATE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EDR-60.134	UV CHANNEL 1 EFFLUENT GATE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-60.210	UV CHANNEL 2 INFLUENT GATE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-60.234	UV CHANNEL 2 EFFLUENT GATE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-60.310	PLANT WATER PUMP STATION INLET GATE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-60.324	3W PUMP 1 DISCHARGE VALVE		NEW	DUTY		1.0	HP
EDR-60.334	3W PUMP 2 DISCHARGE VALVE		NEW	DUTY		1.0	HP
GUH-60-951	3W ROOM GAS INFRA-RED TUBE HEATER		NEW	DUTY		5.5	AMP
GUH-60-952	BLOWER ROOM GAS INFRA-RED TUBE HEATER		NEW	DUTY		5.5	AMP

Date/Time displayed in this report reflect time in PST

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
120	1	LP-60-01	Ν	Indoor
120	0	LP-60-01	Ν	Indoor
480	3	PB-60-01	Ν	Indoor
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-02	Ν	Indoor
480	3	PB-60-02	Ν	Indoor
480	3	PB-60-01	Ν	Indoor
480	0	PB-60-03	Ν	Indoor
480	0	PB-60-02	Ν	Indoor
120	1	LP-60-01	Ν	Indoor
120	1	LP-60-01	Ν	Indoor





PROJECT INFO	RMATION											
P												
PROJECT												
TAG		SPEC SECTION	STATUS	SERVICE			LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
TPV-60.001		22_42_01	NEW	DUTY		0.3	AMP	120	1	LP-60-01	N	Indoor
SF-60.932	3W ROOM SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.3	HP	480	3	MCC-60B	Ν	Indoor
				STANDBY		30.0		480	3	PR-60-01	N	Indoor
HP-60.942	DISINE ECTION HEAT PUMP 2					30.9		480	3	PB-60-01	N	Indoor
DMD 60 330		43 24 50 10				40.0		480	3		N	Indoor
General	Comments: ETAP TAG NPW-60 02	43_24_30.10		Don		40.0	111	400	5	MCC-00D	IN IN	indoor
PMP-60.320	3W PUMP 1	43 24 50.10	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-60A	Ν	Indoor
General	Comments: ETAP TAG NPW-60.01											
EF-60.922	3W ROOM EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.3	HP	120	1	LP-60-01	Ν	Indoor
General	Comments: 1,500 CFM ROOF MOUNTED SUPPLY FAN											
PPU-60.971	ELECT & CNTRL ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-60-01	Ν	Indoor
VCP-60-960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	7.4	AMP	480	3	PB-60-01	Ν	Indoor
UVR-60.211	UV CHANNEL 2, REACTOR 1	43_32_64	NEW	DUTY		37.5	AMP	480	3	MCC-60B	Y	Indoor
General	Comments: ETAP TAG UV PDC-60.03											
UVR-60.221	UV CHANNEL 2, REACTOR 2	43_32_64	NEW	DUTY		37.5	AMP	480	3	MCC-60B	Y	Indoor
General	Comments: ETAP TAG UV PDC-60.04											
EF-60.921	BLOWER ROOM EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-60A	Ν	Indoor
General	Comments: 2,500 CFM ROOF MOUNTED EXHUAST FAN					005.0		400	2		•	
MTS-60-01			NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-60B	N	Indoor
SF-60.931	BLOWER ROOM SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-60A	Ν	Indoor
		12 22 64				27 5		490	2		V	Indoor
Ceneral	Commente: ETAP TAG UV PDC-60.01	43_32_04		DOTT		57.5	AWIF	480	5	MCC-00A	1	muoor
UVR-60 121	UV CHANNEL 1 REACTOR 2	43 32 64	NEW	DUTY		37.5	AMP	480	3	MCC-60A	Y	Indoor
General	Comments: ETAP TAG UV PDC-60.02	10_02_01		Don		01.0	,	100	0			indoor
61 POST AERA	ATION BASIN AND EFFLUENT PUMPING											

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TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
EDM-61.311	BLOWER 1 AMBIENT AIR SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDM-61.321	BLOWER 2 AMBIENT AIR SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-61.110	PAB 1 GATE 1		NEW	DUTY	CONSTANT SPEED	1.0	HP
EDR-61.111	PAB 1 GATE 2		NEW	DUTY	CONSTANT SPEED	1.0	HP
EDR-61.113	PAB 1 DIFFUSER VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-61.210	PAB 2 GATE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-61.211	PAB 2 GATE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-61.213	PAB 2 DIFFUSER VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-02	Ν	Indoor
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-03	Ν	Indoor
480	3	PB-60-02	Ν	Indoor
480	3	PB-60-02	Ν	Indoor
480	3	PB-60-02	Ν	Indoor





PROJECT INFORM	ATION											
PROJE	ECT											
	ATE 5/24/2017 6:30 DM											
61 PUST AERATIC	IN BASIN AND EFFLUENT PUMPING											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EDR-61.318	BLOWER 1 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-60-03	N	Indoor
EDR-61.328	BLOWER 2 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-60-02	Ν	Indoor
EDR-61.460	EFFLUENT WET WELL GATE		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-60-01	Ν	Indoor
BLO-61.323	POST AERATION BLOWER 2	43_11_19	NEW	DUTY	CONSTANT SPEED	40.0	HP	480	3	MCC-60B	Ν	Indoor
BLO-61.313	POST AERATION BLOWER 1	43_11_19	NEW	DUTY	CONSTANT SPEED	40.0	HP	480	3	MCC-60A	Ν	Indoor
General Com	ments: ETAP TAG BLO-60.110											
PMP-61.430	EFFLUENT PUMP STATION PUMP NO. 2	43_24_50.10	NEW	DUTY	VARIABLE SPEED	75.0	HP	480	3	MCC-60B	Ν	Indoor
General Com	ments: ETAP TAG EPMP-60-02											
PMP-61.420	EFFLUENT PUMP STATION PUMP NO. 1	43_24_50.10	NEW	DUTY	VARIABLE SPEED	75.0	HP	480	3	MCC-60A	Ν	Indoor
General Com	ments: ETAP TAG EPMP-60.01											
PMP-61.450	EFFLUENT PUMP STATION PUMP NO. 4	43_24_50.10	FUTURE	DUTY	VARIABLE SPEED	75.0	HP	480	3	MCC-60B	Ν	Indoor
General Com	ments: ETAP TAG EPMP-60-04											
PMP-61.440	EFFLUENT PUMP STATION PUMP NO. 3	43_24_50.10	NEW	DUTY	VARIABLE SPEED	75.0	HP	480	3	MCC-60A	Ν	Indoor
General Com	ments: ETAP TAG EPMP-60.03											
80 DIGESTERS												
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EAM-80.112	AD 1A - AIRFLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-82-03	Ν	Indoor

170	DECONTRACTION		UIAIUU	OLIVIOL	LOAD IN L	LOAD VALUE	LOAD ONITO
EAM-80.112	AD 1A - AIRFLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EAM-80.162	AD 1B - AIRFLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EAM-80.212	AD 2A - AIRFLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EAM-80.262	AD 2B - AIRFLOW CONTROL VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP
EAM-80.312	AD 3A - AIRFLOW CONTROL VALVE		FUTURE	DUTY	CONSTANT SPEED	1.0	HP
EAM-80.362	AD 3B - AIRFLOW CONTROL VALVE		FUTURE	DUTY	CONSTANT SPEED	1.0	HP
MIX-80.100	AD 1A - HYPERBOLOID MIXER	46_41_10	NEW	DUTY	CONSTANT SPEED	40.0	HP
	General Comments: ETAP TAG MIX-82.101						
MIX-80.150	AD 1B - HYPERBOLOID MIXER	46_41_10	NEW	DUTY	CONSTANT SPEED	40.0	HP
	General Comments: ETAP TAG MIX-82.201						
MIX-80.350	AD 3B - HYPERBOLOID MIXER	46_41_10	FUTURE	DUTY	CONSTANT SPEED	40.0	HP
	General Comments: ETAP TAG MIX-82.203						
MIX-80.300	AD 3A - HYPERBOLOID MIXER	46_41_10	FUTURE	DUTY	CONSTANT SPEED	40.0	HP
	General Comments: FUTURE						
MIX-80.250	AD 2B - HYPERBOLOID MIXER	46_41_10	NEW	DUTY	CONSTANT SPEED	40.0	HP
MIX-80.200	AD 2A - HYPERBOLOID MIXER	46_41_10	NEW	DUTY	CONSTANT SPEED	40.0	HP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-82-03	Ν	Indoor
480	3	PB-82-03	Ν	Indoor
480	3	PB-82-02	Ν	Indoor
480	3	PB-82-02	Ν	Indoor
480	3	PB-82-03	Ν	Indoor
480	3	PB-82-03	Ν	Indoor
480	3	MCC-82A	Ν	Indoor
480	3	MCC-82A	Ν	Indoor
480	3	MCC-82B	Ν	Indoor
480	3	MCC-82B	Ν	Indoor
480	3	MCC-82B	Ν	Indoor
480	3	MCC-82B	Ν	Indoor





PROJECT INFORMATION	ON						
PROJECT							
PROJECT NUMBER							
	ANDREW REA						
TAG		SPEC SECTION	STATUS	SERVICE			
				STANDRY		5.0	
				STANDBY		7.5	
PMS 81 000					CONSTANT SPEED	20.0	
EDD 81 104	MRT 1 MM ISO VALVE 1					20.0	
EDR-81 106						1.0	HD
EDR 91 111						1.0	
				STANDRY		1.0	
EDR-81 134				STANDBY		1.0	HP
EDR-81 136	MBT 2 MM ISO VALVE 2		NEW	STANDBY		1.0	HP
EDR-81 141	MENERANE TANK 2 FEELLENT		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81 155			NEW	STANDBY		1.0	HP
EDR-81 164	MBT 2 DISONARCE AIR VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81 166	MBT 3 MM ISO VALVE 2		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81 171	MEMBRANE TANK 3 FEELUENT		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81 185	MBT 3 DISCHARGE AIR VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81 302	WAS SCREEN 1 SUCTION VALVE		NFW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.306	WAS SCREEN 1 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.322	WAS SCREEN 2 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.326	WAS SCREEN 2 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.351	WAS SCREENS MM ISO VALVE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.352	WAS SCREENS MM ISO VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.361	DIGESTER 1 INFLUENT CONTROL VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.362	DIGESTER 2 INFLUENT CONTROL VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.363	DIGESTER 3 INFLUENT CONTROL VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.419	MEMBRANE AIR SCOUR BLOWER 1 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.429	MEMBRANE AIR SCOUR BLOWER 2 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.439	MEMBRANE AIR SCOUR BLOWER 3 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.449	MEMBRANE AIR SCOUR BLOWER 4 DISCHARGE VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.451	MEMBRANE AIR SCOUR DISCHARGE VALVE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.452	MEMBRANE AIR SCOUR DISCHARGE VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-81.453	MEMBRANE AIR SCOUR DISCHARGE VALVE 3		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
GUH-81.951	BLOWER ROOM GAS INFRA-RED HIGH INTENSITY HEATER	23_83_01	NEW	DUTY		5.5	AMP
GUH-81.952	BLOWER ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP
HP-81.941	MT BLDG HEAT PUMP 1		NEW	DUTY		15.3	AMP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-81-01	Ν	Indoor
480	3	PB-81-01	Ν	Indoor
480	3	PB-81-01	Ν	Indoor
120	1	LP-81-01	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-03	N	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	N	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-02	N	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-02	N	Indoor
480	3	PB-81-03	Ν	Indoor
480	3	PB-81-03	N	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-02	N	Indoor
480	3	PB-81-02	Ν	Indoor
480	3	PB-81-03	N	Indoor
480	3	PB-81-02	Ν	Indoor
120	1	LP-81-01	N	Indoor
120	1	LP-81-01	Ν	Indoor
480	3	PB-81-01	N	Indoor





PROJECT INFORMATI	PROJECT INFORMATION											
PROJECT CLIENT PROJECT NUMBER												
REPORT BY	ANDREW REX											
REPORT DATE	5/24/2017 6:30 PM											
81 DIGESTER THICK	ENING BUILDING											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
HP-81.942	MT BLDG HEAT PUMP 2		NEW	STANDBY		15.3	AMP	480	3	PB-81-01	N	Indoor
PPU-81.971	ELECTRICAL ROOM PPU	23_41_51	NEW	DUTY	VARIABLE SPEED	1.5	HP	480	3	PB-81-01	N	Indoor
SF-81.931	STAIRWELL SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP	120	1	LP-81-01	N	Indoor
TPV-81.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-81-01	N	Indoor
VCP-81.960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	7.4	AMP	480	3	PB-81-01	Ν	Indoor
BLO-81.411	AIR SCOUR BLOWER 1		NEW	DUTY	VARIABLE SPEED	30.0	HP	480	3	MCC-81	Ν	Indoor
General Comment	ts: ETAP TAG COMP-81-01	40 00 57 40				5.0	UD	400	2	NOC 04	N	lu da au
PMP-81.213		43_23_57.10	NEW	DUTY		5.0	HP	480	3	MCC-81	N	Indoor
BLU-81.421		40 00 57 40	NEW	DUTY		30.0	HP	480	3	MCC-81	N	Indoor
PMP-81.223		43_23_57.10	NEW			5.0	HP	480	3	MCC-81	N	Indoor
BLU-01.431		40.00 57.40		STANDBY		50.0		460	3		IN	Indoor
PMP-81.233	PERMEATE PUMP 3	43_23_57.10	INEVV	STANDBY	VARIABLE SPEED	5.0	HP	480	3	MCC-81	IN	Indoor
BLO-81 441	AIR SCOUR BLOWER 4		FUTURE		VARIABLE SPEED	30.0	HP	480	3	MCC-81	N	Indoor
PMP-81 243		43 23 57 10	FUTURE		VARIABLE SPEED	5.0	HP	480	3	MCC-81	N	Indoor
1 101 -01.243		45_25_57.10		STANDRY		5.0		480	3		N	Indoor
General Comment	ts: FTAP TAG RUD-81 01			STANDDI	CONSTANT SI LED	5.0	111	400	5	1 0-01-01	IN	indoor
	ROLLUP DOOR 81 (EAST)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-81-01	Ν	Indoor
General Comment	ts: ETAP TAG RUD-81.01											
SCR-81.325	WAS SCREEN 2	46_21_90	NEW	STANDBY	CONSTANT SPEED	5.0	HP	480	3	MCC-81	Ν	Indoor
SCR-81.305	WAS SCREEN 1	46_21_90	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-81	Ν	Indoor
General Comment	ts: PROVIDE 15A CIRCUIT TO VCP. ETAP TAG PMP-81.321	00.04.04				0.0	110	400	<u></u>	1400.04		
EF-81.921	BLOWER ROOM EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	3.0	HP	480	3	MCC-81	N	Indoor
EF-81.922	BLOWER ROOM EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	3.0	HP	480	3	MCC-81	N	Indoor
EF-81.923	SCREENING ROOM EXHAUST FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	MCC-81	Ν	Indoor
MALL-81 911		23 83 05	NEW		CONSTANT SPEED	5.0	HP	480	3	MCC-81	N	Indoor
		20_00_00		2011		0.0		100	Ū			
82 DIGESTER CONTR												
TAG		SPEC SECTION	STATUS	SERVICE				VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
DMC 02 000			NEW	DUTY	CONSTANT SPEED	10.0	HP	480	3	PB-82-01	N	Indoor
						20.0		120	2		IN N	Indoor
						1.0		480	3	PD-02-U3	IN N	Indoor
						1.0		480	3		IN N	Indoor
			FUTURE	DUTY		1.0	HP	480	3	PB-82-03	N	
EDR-82.105	BEP FEED PUMP SUCTION HEADER ISO VALVE 1		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-82-03	N	Indoor

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PROJECT INFORMATIC	N						
PROJECT							
CLIENT							
PROJECT NUMBER							
REPORT BY	ANDREW REX						
REPORT DATE	5/24/2017 6:30 PM						
82 DIGESTER CONTR	OL BUILDING						
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	I OAD TYPE		LOAD UNITS
EDR-82.106	BFP FEED PUMP SUCTION HEADER ISO VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.107	BFP FEED PUMP SUCTION HEADER ISO VALVE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.108	BFP FEED PUMP SUCTION HEADER ISO VALVE 4		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.111	BFP FEED PUMP 1 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.115	BFP FEED PUMP 1 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.121	BFP FEED PUMP 2 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.125	BFP FEED PUMP 2 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.131	BFP FEED PUMP 3 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.135	BFP FEED PUMP 3 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.141	BFP FEED PUMP 4 SUCTION VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.145	BFP FEED PUMP 4 DISCHARGE VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.190	BFP FEED PUMP DISCHARGE HEADER ISO VALVE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.192	BFP FEED PUMP DISCHARGE HEADER ISO VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.194	BFP FEED PUMP DISCHARGE HEADER ISO VALVE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.196	BFP FEED PUMP DISCHARGE HEADER ISO VALVE 4		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.205	MBT FEED PUMP SUCTION HEADER ISO VALVE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.206	MBT FEED PUMP SUCTION HEADER ISO VALVE 2		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.207	MBT FEED PUMP SUCTION HEADER ISO VALVE 3		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.208	MBT FEED PUMP SUCTION HEADER ISO VALVE 4		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.211	MBT FEED PUMP 1 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.215	MBT FEED PUMP 1 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.221	MBT FEED PUMP 2 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.225	MBT FEED PUMP 2 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.231	MBT FEED PUMP 3 SUCTION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.235	MBT FEED PUMP 3 DISCHARGE VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.241	MBT FEED PUMP 4 SUCTION VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.245	MBT FEED PUMP 4 DISCHARGE VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.251	MBT TANK 1 ISO VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.252	MBT FEED PUMP DISCHARGE HEADER ISO VALVE 1		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.253	MBT TANK 2 ISO VALVE B		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.254	MBT TANK 2 ISO VALVE A		NEW	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.255	MBT FEED PUMP DISCHARGE HEADER ISO VALVE 2		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
EDR-82.256	MBT TANK 3 ISO VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP
HP-82.943	DP BLDG HEAT PUMP 3		NEW	STANDBY		26.5	AMP
SF-82.931	STAIRWELL SUPPLY FAN	23_34_01	NEW	DUTY	CONSTANT SPEED	0.5	HP

Date/Time displayed in this report reflect time in PST

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-82-03	Ν	Indoor
480	3	PB-82-02	Ν	Indoor
480	3	PB-82-02	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-05	Ν	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-05	N	Indoor
480	3	PB-82-04	Ν	Indoor
480	3	PB-82-04	N	Indoor
480	3	PB-82-01	Ν	Indoor
120	1	LP-82-01	N	Indoor





PROJECT	INFORMATIC	ON CONTRACTOR OF CONTRACTOR											
	PROJECT												
	CLIENT												
PRC	DJECT NUMBER												
	REPORT BY	ANDREW REX											
	REPORT DATE	5/24/2017 6:30 PM											
82 DIGES	TER CONTR	OL BUILDING											
TAG		DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
TPV-82.001		ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-82-01	Ν	Indoor
VCP-82.960		WATER PUMPS (3) FOR HEAT PUMPS	23_21_23	NEW	DUTY	VARIABLE SPEED	15.2	AMP	480	3	PB-82-01	Ν	Indoor
HP-82.942		DP BLDG HEAT PUMP 2		NEW	DUTY		26.5	AMP	480	3	PB-82-01	Ν	Indoor
HP-82.941		DP BLDG HEAT PUMP 1		NEW	DUTY		26.5	AMP	480	3	PB-82-01	Ν	Indoor
PPU-82.972		CONTROL ROOM PPU	23_41_51	NEW	DUTY	VARIABLE SPEED	1.5	HP	480	3	PB-82-01	Ν	Indoor
PPU-82.971		ELECTRICAL ROOM PPU	23_41_51	NEW	DUTY	VARIABLE SPEED	1.5	HP	480	3	PB-82-01	N	Indoor
EF-82.922		PUMP ROOM EXHAUST FAN 2	23_34_01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-82B	Ν	Indoor
C	General Comments	: CENTRIFUGAL ROOF-MOUNTED UPBLAST EXHAUST FAN											
		ROLLUP DOOR 82 (EAST)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-82-01	Ν	Indoor
	General Comments	: ETAP TAG RUD-81.01											
PMP-82.113		BFP FEED PUMP 1	43_23_57.10	NEW	DUTY	VARIABLE SPEED	30.0	HP	480	3	MCC-82A	Ν	Indoor
(General Comments	:: ETAP TAG BFP-20.01											
PMP-82.123		BFP FEED PUMP 2	43_23_57.10	NEW	DUTY	VARIABLE SPEED	30.0	HP	480	3	MCC-82A	Ν	Indoor
	General Comments	ETAP TAG BFP-82.02	10 00 57 10				05.0		(00	0	100.001		
PMP-82.213	Conorol Commonto		43_23_57.10	NEW	DUTY	VARIABLE SPEED	25.0	HP	480	3	MCC-82A	N	Indoor
DMD 82 222	General Comments	MRT FEED DUMD 2	43 23 57 10		עדוום		25.0	ЦD	480	3	MCC 82A	N	Indoor
FINIF-02.223	General Comments	ETAP TAG PMP-82 02	43_23_57.10		DOTT	VARIABLE SPEED	25.0	nr	460	5	WICC-02A	IN	IIIUUUI
EF-82.921		PUMP ROOM EXHAUST FAN 1	23 34 01	NEW	DUTY	CONSTANT SPEED	0.8	HP	480	3	MCC-82A	Ν	Indoor
	General Comments	CENTRIFUGAL ROOF-MOUNTED UPBLAST EXHAUST FAN								-			
PMP-82.243		MBT FEED PUMP 4	43 23 57.10	FUTURE	DUTY	VARIABLE SPEED	25.0	HP	480	3	MCC-82B	N	Indoor
C	General Comments	: ETAP TAG PMP-82.04											
PMP-82.233		MBT FEED PUMP 3	43_23_57.10	NEW	STANDBY	VARIABLE SPEED	25.0	HP	480	3	MCC-82B	Ν	Indoor
0	General Comments	ETAP TAG PMP-82.03											
PMP-82.143		BFP FEED PUMP 4	43_23_57.10	FUTURE	STANDBY	VARIABLE SPEED	30.0	HP	480	3	MCC-82B	Ν	Indoor
MAU-82.911		PUMP ROOM MAKEUP AIR UNIT	23_83_05	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	PB-82-01	Ν	Indoor
PMP-82.133		BFP FEED PUMP 3	43_23_57.10	NEW	STANDBY	VARIABLE SPEED	30.0	HP	480	3	MCC-82B	Ν	Indoor
C	General Comments	ETAP TAG BFP-20.03											
MTS-82-01		MANUAL TRANSFER SWITCH		NEW	STANDBY	CONSTANT SPEED	225.0	AMP	480	3	MCC-82B	N	Indoor

83 | DIGESTER BLOWER BUILDING

TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS
GUH-83.951	BLOWER ROOM GAS INFRA-RED TUBE HEATER	23_83_01	NEW	DUTY		5.5	AMP
GUH-83.952	BLOWER ROOM GAS INFRA-RED TUBE HEATER		NEW	DUTY		5.5	AMP
TPV-83.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP
VCP-83.122	DIGESTER BLOWER NO. 2 VENDOR CONTROL PANEL		NEW	DUTY		10.0	AMP
VCP-83.142	DIGESTER BLOWER NO. 4 VENDOR CONTROL PANEL		FUTURE	STANDBY		10.0	AMP

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
120	1	LP-82-01	Ν	Indoor
120	1	LP-82-01	Ν	Indoor
120	1	LP-82-01	Ν	Indoor
480	3	MCC-82A	Ν	Indoor
480	3	MCC-82B	Ν	Indoor





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	REPORT DATE	5/24/2017 6:30 PM											
83 DIGE	STER BLOWE	R BUILDING											
TAG		DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
BLO-83.131		DIGESTER BLOWER 3	43_11_38	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-82B	Ν	Indoor
EDR-83.135		DIGESTER BLOWER NO. 3 DISCHARGE ISOLATION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-82-02	Y	Indoor
BLO-83.111		DIGESTER BLOWER 1	43_11_38	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-82A	Ν	Indoor
BLO-83.121		DIGESTER BLOWER 2	43_11_38	NEW	DUTY	VARIABLE SPEED	300.0	HP	480	3	SWG-82A	Ν	Indoor
BLO-83.141		DIGESTER BLOWER 4	43_11_38	FUTURE	STANDBY	VARIABLE SPEED	300.0	HP	480	3	SWG-82B	Ν	Indoor
EDR-83.125		DIGESTER BLOWER NO. 2 DISCHARGE ISOLATION VALVE		NEW	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-82-03	Y	Indoor
EDR-83.115		DIGESTER BLOWER NO. 1 DISCHARGE ISOLATION VALVE		NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	PB-82-03	Y	Indoor
EDR-83.145		DIGESTER BLOWER NO. 4 DISCHARGE ISOLATION VALVE		FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	PB-82-02	Y	Indoor
EF-83.922		BLOWER ROOM EXHAUST FAN 2	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-82B	Y	Indoor
	General Comments	s: HOODED ROOF-MOUNTED EXHAUST FAN											
EF-83.924		BLOWER ROOM EXHAUST FAN 4	23_34_01	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-82B	Ν	Indoor
		ROLLUP DOOR 83 (SOUTH)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-82-01	Ν	Indoor
	General Comments	s: ETAP TAG RUD-81.01											
SF-83.932		BLOWER ROOM SUPPLY FAN 2	23_34_01	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-82B	Ν	Indoor
	General Comments	S: FILTERED LOUVERED ROOM SUPPLY FAN											
SF-83.934			23_34_01	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-82B	N	Indoor
	General Comments	S: FILTERED LOUVERED ROOF SUPPLY FAN			DUTY		10.0		490	2	MCC 924	N	Indoor
VCP-03.112		DIGESTER BLOWER NO. 1 VENDOR CONTROL PANEL			DUTY		10.0		480	2	MCC 92R	IN N	Indoor
VCP-83.132		DIGESTER BLOWER NO. 3 VENDOR CONTROL PANEL	00 04 04	NEW	DUTY		10.0	AMP	480	3	MCC-82B	N	Indoor
EF-83.921	Conoral Commonte		23_34_01	INEVV	DUTY	CONSTANT SPEED	2.0	HP	480	3	MCC-82A	Ŷ	Indoor
EE 83 023	General Comments	BLOWED DOOM EXHAUST FAN 3	23 34 01		עדווס		2.0	ЦD	480	3	MCC 82A	V	Indoor
LI-05.925	General Comments	S' HOODED ROOF-MOUNTED EXHAUST FAN	25_54_01		DOTT	CONSTANT SPEED	2.0	LIE	400	5	WICC-02A		muoor
SF-83.931	Contra Commente	BLOWER ROOM SUPPLY FAN 1	23 34 01	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-82A	N	Indoor
SE-83 933		BLOWER ROOM SUPPLY FAN 3	23 34 01	NEW		CONSTANT SPEED	5.0	HP	480	3	MCC-82A	N	Indoor
	General Comments	s: FILTERED LOUVERED ROOF SUPPLY FAN								-			

85 DEWATERING BUILDING										
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS			
ALP-85.323	EMERGENCY SHOWER/EYEWASH STATION INSTANTANEOUS HOT WATER HEATER	22_42_01	NEW	DUTY		108.0	KW			
BMS-85.900	DEWATERING BLDG BMS CONTROL PANEL		NEW	DUTY		20.0	AMP			
DW-MISC	LIGHTING AND MISC. AT DEWATERING BUILDING		NEW	DUTY		15.0	KVA			
EDR-85.117	BFP1 MM ISO VALVE 1		NEW	STANDBY		1.0	HP			
EDR-85.119	BFP1 MM ISO VALVE 2		NEW	STANDBY		1.0	HP			
EDR-85.127	BFP2 MM ISO VALVE 1		NEW	STANDBY		1.0	HP			
EDR-85.129	BFP2 MM ISO VALVE 2		NEW	STANDBY		1.0	HP			

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VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
480	3	PB-85-02	Ν	Indoor
120	1	LP-85-02	Ν	Indoor
208	3	LP-85-02	Y	Indoor
480	3	PB-85-02	Ν	Indoor
480	3	PB-85-02	Ν	Indoor
480	3	PB-85-02	Ν	Indoor
480	3	PB-85-02	Ν	Indoor





PROJECT INFORMA	TION											
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REPORT E	BY ANDREW REX											
REPORT DAT	FE 5/24/2017 6:30 PM											
85 DEWATERING B	UILDING											
TAG	DESCRIPTION	SPEC SECTION	STATUS	SERVICE	LOAD TYPE	LOAD VALUE	LOAD UNITS	VOLTS	PHASE	POWER SOURCE	GEN POWER	ENVIRONMENT
EF-85.921	POLYMER ROOM EXHAUST FAN		NEW	DUTY	CONSTANT SPEED	0.5	HP	120	1	LP-85-01	Ν	Indoor
FAN-86.810	BIOSOLIDS PAD FAN		NEW	DUTY	VARIABLE SPEED	2.0	HP	480	3	PB-85-01	Ν	Indoor
FAN-86.820	BIOSOLIDS PAD FAN		NEW	DUTY	VARIABLE SPEED	2.0	HP	480	3	PB-85-01	Ν	Indoor
FAN-86.830	BIOSOLIDS PAD FAN		NEW	DUTY	VARIABLE SPEED	2.0	HP	480	3	PB-85-01	Ν	Indoor
GUH-85.951	POLYMER ROOM GAS UNIT HEATER	23_83_01	NEW	DUTY		1.9	AMP	120	1	LP-85-02	Ν	Indoor
GUH-85.952	POLYMER ROOM GAS UNIT HEATER	23_83_01	NEW	DUTY		1.9	AMP	120	1	LP-85-02	Ν	Indoor
PMP-85.361	POLYMER ROOM SUBMERSIBLE PUMP 1	43_25_00.10	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	PB-85-01	Ν	Indoor
PMP-85.362	POLYMER ROOM SUBMERSIBLE PUMP 2	43_25_00.10	NEW	DUTY	CONSTANT SPEED	2.0	HP	480	3	PB-85-01	Ν	Indoor
TPV-85.001	ELECTRONIC TRAP PRIMER ASSEMBLY	22_42_01	NEW	DUTY	CONSTANT SPEED	0.3	AMP	120	1	LP-85-01	Ν	Indoor
General Comm	ROLLUP DOOR 85A (WEST) ents: ETAP TAG RUD-81.01		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-85-02	Ν	Indoor
Conoral Comm	ROLLUP DOOR 85B (MIDDLE)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-85-02	Ν	Indoor
General Comm	ROLLUP DOOR 85C (FAST)		NEW	STANDBY	CONSTANT SPEED	0.8	HP	480	3	PB-85-01	N	Indoor
General Comm	ents: ETAP TAG RUD-85.01		11211	OTABET	CONCIMINIT OF LED	0.0		400	Ū			indoor
PPU-85.971	ELECT ROOM POSITIVE PRESSURIZATION UNIT	23 41 51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-85-01	Ν	Indoor
PPU-85.972	CNTRL ROOM POSITIVE PRESSURIZATION UNIT	23_41_51	NEW	DUTY	CONSTANT SPEED	1.5	HP	480	3	PB-85-01	Ν	Indoor
PMP-85.210	WASHWATER BOOSTER PUMP 1	46_76_21	NEW	DUTY	CONSTANT SPEED	20.0	HP	480	3	MCC-85	Ν	Indoor
PMP-85.111	HYDRAULIC PUMP 1	46_76_21	NEW	DUTY	VARIABLE SPEED	2.0	HP	480	3	MCC-85	Y	Indoor
MTR-85.112	FEED BOX PADDLE MOTOR	46_76_21	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	MCC-85	Ν	
MTR-85.113	GBT DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	N	
MTR-85.114	PRESS 1M-1 DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	
MTR-85.115	PRESS 1M-2 DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	
PBU-85.330	POLYMER BLENDER UNIT 1	46_33_35	NEW	DUTY	VARIABLE SPEED	1.0	HP	120	1	LP-85-02	Ν	Indoor
PBU-85.340	POLYMER BLENDER UNIT 2	46_33_35	NEW	DUTY	VARIABLE SPEED	1.0	HP	120	1	LP-85-02	Ν	Indoor
PBU-85.350	POLYMER BLENDER UNIT 3	46_33_35	FUTURE	STANDBY	VARIABLE SPEED	1.0	HP	120	1	LP-85-02	Ν	Indoor
PMP-85.220	WASHWATER BOOSTER PUMP 2	46_76_21	NEW	DUTY	CONSTANT SPEED	20.0	HP	480	3	MCC-85	Ν	Indoor
PMP-85.121	HYDRAULIC PUMP 2	46_76_21	NEW	DUTY	VARIABLE SPEED	2.0	HP	480	3	MCC-85	Y	Indoor
MTR-85.122	FEED BOX PADDLE MOTOR	46_76_21	NEW	DUTY	CONSTANT SPEED	1.0	HP	480	3	MCC-85	Ν	
MTR-85.123	GBT DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	
MTR-85.124	PRESS 2M-1 DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	N	
MTR-85.125	PRESS 2M-2 DRIVE	46_76_21	NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	
PMP-85.230	WASHWATER BOOSTER PUMP 3	46_76_21	FUTURE	STANDBY	CONSTANT SPEED	20.0	HP	480	3	MCC-85	N	Indoor
PMP-85.131	HYDRAULIC PUMP 3	46_76_21	FUTURE	STANDBY	VARIABLE SPEED	2.0	HP	480	3	MCC-85	Y	Indoor
MTR-85.132	FEED BOX PADDLE MOTOR	46_76_21	FUTURE	STANDBY	CONSTANT SPEED	1.0	HP	480	3	MCC-85	N	
MTR-85.133	GBT DRIVE	46_76_21	FUTURE	STANDBY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	

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PROJECT INFORMAT	ION											
PROJECT												
CLIENT												
REPORT BY												
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IAG MTD 85 134		A6 76 21	SIAIUS	SERVICE				VOLIS	PHASE			ENVIRONMENT
MTD 95 135		40_70_21	EUTURE	STANDBY		5.0		480	3	MCC 85	N	
MIX 95 210		40_70_21	NEW	DUTY		3.0		480	3	MCC-85	IN NI	Indoor
MIX-65.310		40_41_12		DUTY		3.0		460	3	MCC-05	IN NI	Indoor
MIX-85.320	POLYMER TANK MIXER 2	46_41_12	NEW	DUTY	CONSTANT SPEED	3.0	HP	480	3	MCC-85	Ν	Indoor
CON-85.410	DEWATERING BELT CONVEYOR		NEW	DUTY	CONSTANT SPEED	5.0	HP	480	3	MCC-85	Ν	Indoor
HP-85.941	DB HEAT PUMP 1		NEW	DUTY		19.7	AMP	480	3	PB-85-01	Ν	Indoor
VCP-85.960	WATER PUMPS (2) FOR HEAT PUMPS	23_21_23	NEW	DUTY		7.4	AMP	480	3	PB-85-01	Ν	Indoor
HP-85.942	DB HEAT PUMP 2		NEW	STANDBY		19.7	AMP	480	3	PB-85-01	Ν	Indoor
EF-85.922	DEWATERING BLDG FUME EXHAUST FAN	23_34_01	NEW	DUTY	VARIABLE SPEED	50.0	HP	480	3	MCC-85	Ν	Indoor
MAU-85.911	DEWATERING BLDG MAKEUP AIR UNIT	23_83_05	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-85	Ν	Indoor
FAN-85.891	ODOR CONTROL FOUL AIR FAN 1	23_34_17	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-85	Ν	Indoor
General Commer	nts: FAN-85.991 IS NOW PART OF BID ALTERNATE.											
FAN-85.892	ODOR CONTROL FOUL AIR FAN 2	23_34_17	NEW	DUTY	VARIABLE SPEED	40.0	HP	480	3	MCC-85	Ν	Indoor
General Commer	nts: FAN-85.992 IS NOW PART OF BID ALTERNATE.											
FAN-85.893	ODOR CONTROL FOUL AIR FAN 3	23_34_17	NEW	STANDBY	VARIABLE SPEED	40.0	HP	480	3	MCC-85	Ν	Indoor
General Commer	ts: FAN-85.993 IS NOW PART OF BID ALTERNATE.											

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ELECTRICAL	ELECTRICAL									
Motor Control Centers										
Designation:	Cutler Hammer									
Manufacturers:										
Communications:	DeviceNet									
Thermal Magnetic Breakers	Thermal Magnetic Breakers, not Motor Circuit Protectors									
Variable Frequency Drives - Low Voltage										
Manufacturers:	Cutler-Hammer									
Communications:	DeviceNet									
Fail-safe System										
Requirements:	None									
Philosophy for fail-safe systems?	System is dual pov	wer fed, Generator on site – load shed required								
Lightning Panels										
Manufacturers:	No preference									
Notes:	SPDs required at e	each panel								
Voltage Requirements:	240/120VAC – So	me locations vary								
Conductors										
Color coding:	BYO									
Insulation Class:	THHN for control v	vires								
Labeling:	?									
Motor winding hea	aters									
Motors located inside:	No									
Motors located outside:	No									
Horsepower Constraints:	No									
Uninterruptible Po	wer Supplies	5								
Manufacturer:	Manufacturer: APC – On line units									
Location:	Centralized:	Centralized UPS in the control room□								
	Distributed:	Distributed in PAC cabinets								
Back-up Time:	15-20 Minutes									
Alarms:	Discrete Alarms									
Network communication:	None									
Disconnects										

Process Motors:	Y			
HVAC:	Y			
Instruments:	N			
Position indication:	Ν			
Power Monitoring				
Designation:				
Manufacturers:	CH Power Expert.			
Network communications:	Ethernet is desired – CH communications is not Ethernet based.			
Desired Data:	Phase-Phase Voltage, KW, PF, Phase Current, No Harmonics.			
Locations:				
Generators and Po	ower Failures			
Manufacturers:	Wakashaws 300KW – Qty 2			
Fuel Type:	Duel Fule – Natural gas and Methane			
Fuel Storage:	1000 Gal/Generator			
Network communications:	None			
Data:				
Secondary Power Source:				
Loss of power generator start:	Manual			
Return to primary power:	Manual			
Source Transfer	Open Cogen			
Transition:	Closed ?			
Load shed require	ments?			
Load shedding is required -	- Generators are not sized to pick up all plant loads			
Information from o	other specific loads (UV system, etc)?			
Lightning - Outdo	or			
Outdoor lightning lamp s	tyle: Metal halide			

Does the client follow Dark	Sky Yes				
Is lighting required to variation around or to work	walk Yes k in?				
Lightning - Indoor					
Indoor lighting lamp style:	Metal halide				
Emergency lights or	Yes Emergency lighting is deployed.				
battery backup in fixtures?	Yes Night lights are used.				
Conduit Systems					
List material preferences	PCS – Commonly used				
for corrosive areas:	PVC – Commonly used				
List material preferences	Aluminum - Optional for Exposed areas				
for non-corrosive areas:	Galvanized steel – Commonly used				
Duct bank Constru	uction				
Separate manholes or hand	holes for the following:				
480VAC, 120VAC and	Separate the 480VAC – Analog and discrete can share				
Analog.	No				
Electrical Safety	Isolated electrical rooms are desired				
desired?					
Remote control/racking	Needs to be determined				
capacity desired?					
Arc resistant gear	Needs to be determined				
Infrared scanning windows desired? Needs to be determined					
Maintenance switches	Needs to be determined				
desired?					
Discuss arc flash labeling	Needs to be determined				
requirements nere:	Vaal standarda apply				
Coordination					
coordination					
Requirements					
Minimum HP where reduced voltage soft starts are required. None					

Is there a power factor penalty?	Yes
Any installation requirements/details pertinent to the project?	No

DESIGN CHECKLIST: FIELDBUS STANDARDS

FIELDBUS STA	NDARDS		
Digital Bus Field Networks			
DeviceNet:	[X]		
EtherNet/IP:	[X]		
Profibus DP:	[X]		
Profibus PA:	[X]		
Foundation H1:			
Foundation HSE:			
Other:			
Other:			
Communications Mod	dules		
Prosoft:			
SST:			
Other:			
Other:			
Fieldgates			
Endress Hauser Fieldgate			
Repeaters			
Procentec Profihub			
Diagnostic Equipmen	nt		
Profitrace Software with mot	bile communication:		
Profitrace Control Panel h	ardware is desired:		
Procentic	Diagnostic Module:		
Terminators			
Phoenix Conta	ict (screw type DB):		
	Procentec:		
Couplers			
CompactLogix:			
ENTPA:			
ControlLogix:			
P&F PowerHub:			
Profibus Component	Accessories		
Multimaster Control:	ComSoft PRS Switch		

DESIGN CHECKLIST: FIELDBUS STANDARDS

Redundancy Media Module:	RLM					
Fiber Transceivers:	Hirschman OZD					
Terminations						
Valves Profibus DP:	Repeater					
	Manufacturer Hub Hardw	red connections				
Valves Profibus PA:						
Standard PA Junction Box						
Eurofast Connections						
Hardwired						
Instrument Profibus DP						
Eurofast Connections						
Hardwired						
Instrument Profibus I	PA					
Standard PA Junction Box						
Eurofast Connections						
Hardwired						
Profibus DP Configur	ation					
Profibus DP networks connecting field devices will have the following busparameter settings. A baudrate of 187.5k should be used for all Profibus networks extending into the field. A baudrate of 187.5k will allow for electrical Profibus segment lengths of up to 3,250 feet and eliminates many of the noise issues in higher speed networks. Segments can be extended an additional 700 feet by reducing the baudrate to 93.75k. Reducing the baudrate below 93.75k offers no additional segment length and should only be done if there are significant noise issues or bit errors on the network.						
Primary	Master Node Address – 1					
Secondary	Master Node Address – 2					
N	letwork Baudrate – 187.5k					
	Slot Time (T _{SL}) – 1000					
Minimum Station Delay	Responder (minT _{SDR}) – 11					
Maximum Station Delay Re	esponder (maxT _{SDR}) – 800					
	Quiet Time (T _{QUI}) – 9					
	Setup Time (T _{SET}) – 95					
GA	AP Update Factor (G) – 10					

Highest Station Address (HSA) – 126

Max Retry Limit – 5

DESIGN CHECKLIST: FIELDBUS STANDARDS

The values of T_{SL} , max T_{SDR} , and T_{SET} must be configured to the above values when the Pepperl+Fuchs Power Hub DP/PA coupler is used. The GAP Update Factor must be set to 10 for multiple master networks, otherwise secondary masters will never be allowed to respond.

When ABB S800 I/O is used, it will typically operate on its own Profibus DP network. If the only nodes on the network are S800 I/O, the default settings for CI854 modules should be used (differences shown below).

Network Baudrate – 1.5M		
Slot Time $(T_{SL}) - 300$		
Maximum Station Delay Responder (maxT _{SDR}) – 150		
Quiet Time $(T_{QUI}) - 0$		
Setup Time (T _{SET}) – 20		
GAP Update Factor (G) – 1		
Max Retry Limit – 3		
Control Cabinet Standards		

DESIGN CHECKLIST: GENERAL

General			Last Upo	date:	
Client Naming/Tagging Conventions:					
List tagging and loop number convention			See attach	ned	
		Left to Right	Х		
Pilot Devices		_	I		
Control Station Controls L	ocation:	Field:		X	
		PTT		X – No transformer	
		MCC/VFD		X – HIM modules	
Pilot Light Types – loc	ated on Buckets	LED:		X	
		Push to test:		X	
	Red:	Running			
	Green:	Standby/Rea	dy		
	White:	Power On			
	Blue:	2 speed - Rui	n Slow		
Aml	per: Fail	Fault			
Packaged Equ	lipm	ent Pref	erenc	es	
Packaged equip	oment	with star	ters		
Sump Pumps			-		
Starter Location:	Field:		Х		
		MCC:			
Controls:	Plant:				
		Vendor:	Х		
Monitoring:	Plant PCS:		Х		
Level Element Type:	Floats:		Х		
HVAC Air Handling/Make up Air Units/Evaporative Coolers:				aporative Coolers:	
Starter Location:	Field :		Х		
-		MCC:	Х		
Controls:	Plant		Separate	Controls – Soldyn MTEC	
	Vendor		Х		
Monitoring	Plant PCS:		Х		

DESIGN CHECKLIST: GENERAL

Fire Alarms				
Fire Alarm Control Panel:	X			
Third Party Monitored:	No			
Signal Type:	Traditional: X			
	Addressable:			
Security Alarms				
Security system control panel required?	N			
Third party vendor supported?	N			
Local panels:	N			
Card Access:	Entry Gate only – Staff doesn't like			
Security System Software				
Security System Softw				
Security System Softw N/A				
Security System Softwork N/A Security System Hardw	vare			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled	ware Gate Monitoring Only			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements:	ware Gate Monitoring Only No formal standards.			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System	ware Gate Monitoring Only No formal standards.			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone:	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support:	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services City IT maintains phone system - Cisco			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services City IT maintains phone system - Cisco Maintenance takes care of paging system			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services City IT maintains phone system - Cisco Maintenance takes care of paging system Phone system controls through PAX			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System Manufacturer:	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services City IT maintains phone system - Cisco Maintenance takes care of paging system Phone system controls through PAX None.			
Security System Softwork N/A Security System Hardwork CCTV: Internally controlled Physical Installation Requirements: Phone System Phone: Support: Paging System Manufacturer: System Requirements: Energy Management S	vare Gate Monitoring Only No formal standards. VOIP based, CISCO and Clarion City IT services City IT services City IT maintains phone system - Cisco Maintenance takes care of paging system Phone system controls through PAX None. ystem			

DESIGN CHECKLIST: GENERAL

Building Management			
Manufacturer:	Nothing in place.		
Lightning Protection	on:		
Is lightning protection required?	Yes – Ground Rods and Ground Loop		

INSTRUMENTATION		Last Update:			
Instrument Preferences					
Digital Bus Re	quired:	DeviceNet Motor Control – Instruments are pending			
FDT/DTM requirem	nent for ments?	Yes 4-20mA H	HART		
Flow Sv	vitches	No preference			
Flow Meters C	oriolis:	No preference			
Flow Meters Th	nermal:	Sierra			
Flow Meters Ma	gnetic:	Endress+Hause	er 53W		
		Bypass prefere	nce	Spool piece X	
		Spool piece ma	terial	PVC X - Typical	
				Steel X – in special cases	
Level Swi	tches:	Standard Floats	s and Tuning Forks		
Level Ultrasonic instru	ments:	Endress+Hause	er SP1, 4 wire, Integra	l (in most applications)	
Level Radar instru	ments:	No preferences			
Pressure Sw	vitches:	Ashcroft DPDT			
Pressure G	auges:	Ashcroft – 1279 Glycerin filled			
Pressure Transmitters:		Endress+Hauser Cerebar.			
DO:		Endress+Hauser			
pH:		Endress+Hauser			
	ORP:	Endress+Hauser			
Tu	rbidity:	HACH, Endress+Hauser			
Gas Detection:		Sierra Monitor Corp – Sentry Q with remote transmitter		emote transmitter	
Analyzers:		Ammonia: Endress+Hause	er ISOMax	Nitrate: Endress+Hauser ISOMax	
Control Philosophy					
Two Wire (HOA) of desired?	r thre	e-wire (LOF	R+Start/Stop p	ushbuttons) controls	
Three-wire control:	Yes				
Reset preferences:	Reset pushbuttons				
Interlocks					
Software:	Mostly	Software			
Hardware:	Hardware: Where required				
Device Networking	Prefe	erences			

Need to evaluate on a project	t basis if a	applicable based on data needs or economic constraints.	
Non-Modulating valves:			
Modulating valves:			
MCC:	Х		
VFD:	Х		
Switchgear:			
Motor Protection Relays:			
Control Cabinet St	andaro	ds	
Lighting inside control of	cabinets:	X	
Automatically on as door	r opens :	X	
Cabinet Temperature Mo	onitoring:	Switch to start fans – not alarmed	
Intrusion of	contacts:	No	
Alar	m horns:	Control Room Only	
Alarm	Strobes:	On buildings not panels	
Control Panel	Depths:	Colors: Red = Signal, Black = Hot, White = Neutral. Green = Ground Wire shall be stranded MTW	
	Panduit	Grey	
Termina	al Blocks	Screw Terminals	
Analog Termina	al Blocks	Fused (min Fuses), Disconnect and test point.	
	Discrete	Circuit Breaker	
Surge P	rotection	SPD on panels and SPD on field instruments located outside	
Control Pane	l Names	ACC-xx where xx = process area abbreviation	
Ethernet S	Switches	Cisco IE3000 located in the ACC	
Fiber Pat	ch Panel	Located in ACC	
Ve	entilation	Fan vents located on Top front corners on ACC	
Wiring Sta	andards:	Conductor Field Labeling: Tag Based	
		Conductor Panel Labeling: TAG-S-1 (analog) TAG-C-! (discrete)	
		25% spare I/O per card	
Any specific layout standards:		25% spare rack space	
		All spare I/O is wired to filed terminal blocks	
Controller Preferen	nces		
Existing	g system	GE based – Mainly GE RX3i	

Manufacturer preference GE RX3		GE RX3	bi PAC 120VAC		
Processor redundancy required? Not typic		Not typi	cally but could vary based on the installation requirements		
Power Supply Redundancy					
24 VDC:	X				
UPS:	Х				
Fail contacts monitored:	Yes				
I/O Standards: DI a	nd DC):			
24 VDC					
120 VAC					
Isolated Inputs:	Yes				
Isolated Outputs:	PLC cat	oinet X			
Interposing relays location:	Relay C	abinet X			
	Starter >	K			
Analog Voltage	4-20mA				
Communication protocol	IP Back	bone			
preference?	Modbus	TCP			
Field Networks:	Etherne	t is desire	d		
HMIs					
HMI required on PLCs?		n PLCs?	iFix Proficy		
HMI hardware preference?		erence?	No real preference – ACP may be desirable		
PCS/SCADA Prefe	rences	:			
List applicable communicat	tion requir	ements:	Others?		
[Internal/External/Others]		/Others]	Thin client deployment is desired, Thick in control room.		
Will the operator workstations have run-time, development or thin client licenses?		un-time, censes?	Large Process display screen		
Any specific op	erator wo	rkstation	CCTV Display screen(s)		
requirements?		ements?	Currently under review - Firewall exists between corporate in the plant but corporate controls the firewall		

List any currently deployed SCADA security Currently under review - Firewall exists between corporate in measures like firewall rules etc. the plant but corporate controls the firewall Virtualization Requirements: iHistorian - potentially Thin Client Manager SCADA Server Notes Dual SCADA servers - not virtualized one on site and a second offsite. GE Webspace is used and located on the offsite server **Communication System Network** List Internal and External Communication Plant Corporate: VPN on T1 requirements: Control System: VPN access Switches IT for large infrastructure List network preferences for equipment: Equipment furnished by? Cabinet switches by Contractor



		1		ŝ	7		>	0	10	11	10	10		
			2 3 4 5	6	/	6	5	9	10	11	12	13		
l Ir			BILL OF MATERIALS											
-														
-	IEM	MANUFACTURER	DESCRIPTION						2		40 004744			
		Allen-Bradley	MiniStyle Devicenet 5-Pin Female Terminator	1 1485A-T1N5	61	Phoenix Contac	ct	D-UI 2,514-IWIN Terminal C	Cover		12 3047147			
	2	Allen-Bradley	MiniStyle Devicenet Cordset, 5-Pin Male Connector to Cable, 3.3 Feet	1 1485C-P1M5-C	62	Phoenix Contac	ct	UBE/D Terminal Strip Marker	r Carrier		18 800307			
	3	Allen-Bradley	MiniStyle Devicenet T -Port 5 -Pin Devicenet Connector with 1 4-Pin Male Power Drop	1 1485T-P1M4-MN5KF	63	Phoenix Contac	ct	UT4 Terminal Block			148 3044102	2		
AL			Connection		64	Phoenix Contac	ct	UT10 Terminal Block			2 3044160)		
	1	Allen-Bradley	MiniStyle Devicenet T -Port 5 -Pin Devicenet Connector with 1 5-Pin Female Drop	1 1485P-P15-MN5KF	65	Phoenix Contac	ct	UT4 Grounding Terminal Bloc	ck		2 3044128	}		
-	T	Alicit-bradicy	Connection		88	Phoenix Contac	ot ot	LIT4 Grounding Terminal Bloc	ok		2 3044129	}		
▎▕┝			Connection		00						2 3044120)		
	5	Allen-Bradley	MiniStyle Devicenet Cordset, 4-Pin Female Connector to Cable, 6 Feet	1 889N-F4AFC-6F	67	Phoenix Contac	Ct	UI4-MID Terminal Block			57 3046184			
	5	APC	Rack Mounted Automatic Transfer Switch, 120 V AC 15 A	1 AP7750	68	Phoenix Contac	ct	Fused Disconnect Type Tern	ninal Block with Light Indicato	r, 24V DC	34 3046090)		
	7	APC	1000V A Rack Mount Uninterruptible Power Supply with Relay Card	1 SUA1 OOORMI UIAP961 0	68	Phoenix Contac	ct	24V DC 5A Power Supply			2 QUINT/F	S/1 AC/24DC/5		_
	2	Bryant	5-15P 15 Amp 120V AC Plug	1 5266NIP	69	Phoenix Contac	ct	24V DC 10A Power Supply			2 QUINT/F	S/1 AC/24DC/1	0	
1 18	, ,	Diversion	A Straw 20 and Astrono Class Fund		70	Paco		Handy Box and Dupley Boco	ptacle Cover		5 670PAC	/69/		
	1	Bussmann	4A Smmx 20 mm Fast-Acting Glass Fuse	1 GMA-4-R	70						0/0KAC	/004		
	10	Bussmann	2A 5mmx 20 mm Fast-Acting Glass Fuse	9 GMA-2-R	/1	Saginaw		24" Door Activated Fluoresce	ent Light		3 SCE-LF	146D24		
	11	Bussmann	1/2A 5mmx20 mm Fast-Acting Glass Fuse	24 GMA-500-R	72	Siemens		1 Pole, 3A Circuit Breaker			26 5SJ410	3-7HG41		
ЫГ	12	Cisco	Industrial Ethernet Switch, 4 10/100 ports, 2 dual purpose uplink ports	1 IE-3000-4TC	73	Siemens		1 Pole, 6A Circuit Breaker			7 5SJ410	6-7HG41		r
	13	Cisco	Ethernet Expansion Module for IE3000 8 10/100 ports TX Ports	1 IEM-3000-8TM	74	Siemens		1 Pole, 15A Circuit Breaker			4 5SJ4118	3-7HG41		1
	1.4	Custom			75	Siemens		1 Pole 204 Circuit Breaker			2 59 14120)-7HG41		
	14	Custom	Glounding Bar - 1/4 x 1 x Panel Length	2 By Description	76	Ciamana		15" Industrial Calar Flat Dan	al Tauahaaraan Manitar		2 0004120			
	15	Cutler-Hammer	Aegis Surge Protective Device	1 AGSHWCH120N20XC	70	Siemens		15 Industrial Color Flat Falle			1 0AV700	I-ZIBUU-IAAU		
	16	Entrelec	Standard DIN Rail	1 Lot 0101 598.26	77	General Electri	С	IFIX IClient Runtime Software	e		1 IC6471F	CLNICRNM		
Ľľ	17	Entrelec	30 ⁰ Raised DIN Rail	1 Lot 0101 875.23					LEGEND SCHEDU	LE				
 	18	General Electric	Fanuc RX3i Blank Cover	10 IC694ACC310				MATERIAL: G	GRAVOPLY-II, BLACK FIELD W	ITH WHITE 3/16" LETTERS				
-	-	General Electric	Fanue RX3i 10 Slot Expansion Chassis	1 10694049302	— —									$\neg \mid$
-	20	Conoral Electric	Espus DV2i 16 Doint Digital Input Madula, 1201/ AC					LINE 1	LEGEIND	LINE 2		LINE 3		-1
	20						1000					LINE J		-
	21	General Electric	Fanuc RX3i 8 Point Relay Digital Output Module, Isolated	4 IC694MDL930			ACC-		AREA CONTROL C	ENTER				-
الم	22	General Electric	Fanuc RX3i 4 Point Current Analog Input Module, Differential	6 IC695ALG608		PZ 2 X 4	I DEVIC	JEINE I	TO MCC-D1					_ .
	23	General Electric	Fanuc RX3i Terminal Connector for Analog Input Modules	6 IC694TBB032										1
	24	General Electric	Fanuc RX3i 16 Slot Universal Chassis	1 IC695CHS016										
l l i		Conorol Electric	Fando RY3 Expansion Cold of the States	1 IC603CPI 201										
É	20			1 100930BL301					LEGEND SCHED	ULE				
	26	General Electric	Fanuc RX3i Devicenet Communication Module	1 IC694DNM200				MATERIA	AL: GRAVOPLY-II, YELLOW FI	ELD WITH BLACK LETTERS				
	27	General Electric	Fanuc RX3i Expansion Rack Power Supply	1 IC694PWR330										
	28	General Electric	Fanuc RX3i CPU 64MB User RAM w/ Auxiliary Battery	1 IC695CPU320 / IC693ACC3)2						- 7			
	29	General Electric	Fanuc RX3i Ethernet Communication Module	1 IC695FTM001				SIZE TEXT SIZE LINE T	LINE Z	LINE	. J			
	20	Conoral Electric	Equip DY2 Social Expansion Modulo				NP2	2 X 6 1/4 ** SEE L	JETAIL AT RIGHT**					
Ľ	50	General Electric		I ICOSSEREOUT										
▎▕┝														
	31	General Electric	Fanuc RX3i CPU Rack Power Supply	2 IC695PSA140										Ι.
D	32	Graceport	PS 2 /Keyboard/Mouse/USB Interface/RJ45 Interface	1 P-P3P5P11P11R2-B3R0										1
	33	Hoffman	Large Plastic Data Pocket	1 ADP2										
	34	Hoffman	Filter 8 v 14	3 AFI T812										
H) 4		Torse and the Oceanal Outland											
	55	Holiman	Temperature Control Switch											
	36	Hottman	Louver Plate 8 x 14	3 AVK812										
	37	Hoffman	Keyboard Box	1 CKBC24										-
	38	Hoffman	Proline Pull Out Shelf, 19" Deep	2 P19PSH6										
	39	Hoffman	Proline Rack Panel - 6 U	2 P19RP6UP										
	10	Hoffman	Proline 100mm Plinth Base 800 x 800	3 PB188										
L I F	+0													
	+1	Holiman		3 PC3208										
E	+2	Hottman	Proline Solid Door, 2000 X 800	3 PDS208										E
l II	13	Hoffman	Proline Single Bay Frame, 2000 x 800 x 800, Nema-12	3 PF2088										
[14	Hoffman	Proline 1-Hole Grid Strap (Pair)	3 PGH1S8										
[15	Hoffman	Proline G1 and Plate, 800 x 800	2 PGP88										
	16	Hoffman	Proline Frame Joining Gasket Kit	2 P.12F										
H	17	Hoffman	Proline Joining Papel											
Πŀ	10													F
-	+0	nonman												
	19	Hoffman	Proline Full Panel, 2000 x 800	3 PPF208										
	50	Hoffman	Proline 19" Rack Angle, 73" Longwith Tapped Holes (pair)	4 PRA1920TP										
	51	Hoffman	Proline 19" Rack Angle, 22" Longwith Tapped Holes (pair)	1 PRA197TP										
_ [52	Hoffman	Proline Solid Side, 2000 x 800	2 PSS208										
F	52	Hoffman	Proline Vented Ten Een 200 x 200 115 \/ AC	1 D\/T2E994										
	54	Hottman	Proline Solid Top, 800 x 800	2 P188										
	55	ldec	DPDT Relay, 120V AC with Indicator and Base	2 RH2B-UL-AC120/SH2B-05										
	56	ldec	DPDT Relay, 24VDC with indicator and Base	4 RH2B -UL-DC24/SH2B-05										
	57	Leviton	120 V AC. 15A Duplex Receptacle	1 5252-I										
HH	58	Leviton	120 V AC. 20A Duplex Recentacle	1 5352-1										H
	50	Lovitor	154 looloted Cround Dupley Recenterie	2 920010										
	19													
	50	Phoenix Contact	E/UK End S top	12 1201442										
L								· · ·						
G			DESIGNED						CITY O	F BOULDER WWTF		VERIFY SCALES	JOB NO.	
Ľ								F				BAR IS ONE INCH ON	~~~~~	`
L									PROCESS	AUTOMATION SYSTEM	1	ORIGINAL DRAWING	DRAWING NO	10.
										INSTRUMENTATION		0 1"	I-008	
														-
									BO			THIS SHEET, ADJUST	SHEELNO.	·
F	EV DA	TE BY	DESCRIPTION MONTH YEAR							ACC-XXX		SCALES ACCORDINGLY	2 OF X	XX.

_	 	 0

DESCRIPTION

REV DATE

2

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10

CITY OF BOULDER WWT	F	VERIFY SCALES	JOB NO. XXXXX.XX	G	
ROCESS AUTOMATION SYS	DCESS AUTOMATION SYSTEM				
INSTRUMENTATION	0 1"	1-008			
BOULDER WWTF	IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.			
ACC-XXX		SCALES ACCORDINGLY	2 OF XX		
11	12	13			
		Appendix A-	2		

	5 6 7	8 9		12 13	\neg
			ELECTRICAL ONE-LINE STMBOLS		-
IDENTIFICATION SYMBOLS SWITCHES/RECEPTACLES	RACEWAY	MEDIUM VOLTAGE	LOW VOLTAGE	MISCELLANEOUS	
A EQUIP # EQUIPMENT AND INSTRUMENT IDENTIFICATION S A SINGLE POLE SWITCH A = CIRCUIT DESIGNATION b = DEVICE SWITCHED DESIGNATION		a CIRCUIT BREAKER, MEDIUM VOLTAGE a = CIRCUIT BREAKER, MEDIUM VOLTAGE b = FRAME SIZE	e LOW VOLTAGE CIRCUIT BREAKER b O c) a a = TYPE MCP = MOTOR CIRCUIT PROTECTOR	HP HORSEPOWER RATING FULL LOAD AMPS AS NOTED	A
EQUIPMENT/INSTRUMENT LOCATOR 2 = DOUBLE POLE SWITCH 3 = THREE-WAY SWITCH	BREAK AND CONTINUATION IN CONDUIT RUN	a ANSI RELAY DEVICE	d O/ f TM = THERMAL MAGNETIC SS = SOLID STATE b = FRAME SIZE (MANUFACTURER TO DETERMINE FRAME SIZE UNI ESS INDICATED)	a PACKAGED EQUIPMENT	
b x a c CIRCUIT DESIGNATION b = DEVICE SWITCHED FROM b = DEVICE SWITCHED FROM b = DEVICE SWITCHED FROM b = DEVICE SWITCHED FROM c = CIRCUIT DESIGNATION b = DEVICE SWITCHED FROM c = CIRCUIT DESIGNATION c = CIRCUIT	FLOORS OR OTHER STRUCTURES	b a = ANSI DEVICE FUNCTION b = QUANTITY	c = NUMBER OF POLES d = TRIP SETTING (AT = AMP TRIP) (AC = MCP CONTINUOUS RATING)	LOAD RATING AS INDICATED a = RATED LOAD b = UNIT(HP, KW, KVA) AS INDICATED	
c = MOUNTING HEIGHT IN FEET TO BOTTOM OF FIXTURE c = MOUNTING HEIGHT IN FEET TO BOTTOM OF FIXTURE c = MOUNTING HEIGHT IN FEET TO P = SWITCH AND PUBLOT LIGHT T = THERMOSTAT D = DIMMER SWITCH	OR IN DUCT BANK		e = DESIGNATION f = INTERRUPTING RATING		
CONDUIT IDENTIFICATION XXXX = CONDUIT NUMBER, PEEER TO CONDUIT SCHEDINE	CONDUIT VERTICAL CHANGE IN DIRECTION	d	O O O O O O O O O O O O O O O O O O O	$ \begin{array}{c} a = 0 \text{ EVICE LD.} \\ b = \text{ KVA RATING} \\ g \\ g \\ g \\ \end{array} \begin{array}{c} c = \text{ NUMBER OF PHASES} \\ d = \text{ PRIMARY VOLTAGE} \end{array} $	
B B MULTIPLE SWITCH LOGATIONS UNLESS OTHERWISE NOTED, GROUPED CONDUITS ARE LABELED LEFT TO RIGHT OR TOP TO BOTTOM. REFER TO ABBREVIATIONS LEGEND FOR ULL OTHER DESIDENT			= G = GROUND FAULT INTERRUPTER = V = SOLENOID KEY RELEASE	I e e = SECONDARY VOLTAGE h f,g = CONNECTION TYPE SYMBOL h = IMPEDANCE	В
INDICATES KEYNOTE X (PERTAINS ONLY TO SHEET WHERE NOTE IS FOUND) b X a c OCCUPANCY SENSOR C X = REFERENCE I IGHTING CONTROL COMPONENT SCHEDULE	UJUNCTION BOX		 ⊡		
A = THE EVENCE CONTINUE C	CONDUIT TEE	MEDIUM VOLTAGE DISCONNECTING FUSE	DISCONNECT SWITCH A = TYPE, REFER TO DISCONNECT SCHEDULE		
A = TYPE, REFER TO DISCONNECT SCHEDULE (PE) PHOTOCELL		O V DOUBLE FUSE CUT OUT	 	a ENGINE-GENERATOR RATINGS AS INDICATED ON G b THE DRAWINGS C a = KVA/KW d b = VOI TAGE/CONNECTION	
LUMINAIRES -Obassi and the second structure a = CIRCUIT DESIGNATION b = DEPENDENT OF THE DESIGNATION	APPROAIMALE DIMENSIONS SHOWN ON DUCT BANK SECTIONS	MEDIUM VOLTAGE SINGLE FUSE	FUSED DISCONNECT SWITCH B = TYPE REFER TO DISCONNECT SCHEDULE	e c = PHASE d = WIRE e = PF	
$ \begin{array}{ c c } \hline \hline$	CONDUIT SIZE AND CONDUCTORS				c
2' X 2' LAY-IN TROFFER				a = QUANTITY b = RATIO	
2' X 4' LAY-IN TROFFER $ \bigcirc^{a}_{b}$ IN FLOOR DUPLEX RECEPTACLE $ \bigcirc^{a}_{b}$ IN FLOOR QUADRUPLEX RECEPTACLE	W"C-(3-X (Ø), 1-Y (N) & 1-Z (G)) W"C (WHERE INDICATED): W = CONDUIT TRADE SIZE	MEDIUM VOLTAGE LIVE FRONT TERMINATOR	FUSE	$\begin{array}{c} c & a & d \\ \hline \\$	
$\begin{array}{c} & & \\$	3-X (Ø): 3 = QUANTITY X = SIZE OF CONDUCTORS			b b = RATIO c,d = CONNECTION TYPE SYMBOL	\vdash
$ \begin{array}{ c c } \hline & & & & \\ \hline R & & & \\ \hline G & & \\ G & & \\ \hline G & & \\ G & & \\ \hline G & & \\ G & $	(Ø) = DESIGNATES PHASE CONDUCTORS 1-Y (N)(WHERE INDICATED):		a COMBINATION STARTER	SSM SOLID STATE MULTIFUNCTION METER	
H = HORN D RG GO/NO-GO PANEL - SOLID FOR WEI DING RECEDITACIE	1 = QUANTITY Y = SIZE OF CONDUCTORS (N) = DESIGNATES NEUTRAL CONDUCTORS	MEDIUM VOLTAGE TEE	WITH CONTROL POWER TRANSFORMER a = CIRCUIT BREAKER DISCONNECT, b TYPE AS NOTED T c b = STARTER TYPE	ATP AMPERE TEST POINT	D
X B vietuning Recuer Jacket R GO/NO-GO PANEL - STROBE a = CIRCUIT DESIGNATION a b = DISCONNECT TYPE	1-Z (G)(WHERE INDICATED): 1 = QUANTITY Z = SIZE OF CONDUCTORS		d = NEMA STARTER SIZE	VTP VOLTAGE TEST POINT →	
LUMINAIRE, EMERGENCY BATTERY-POWERED	(G) = DESIGNATES GROUND CONDUCTORS U(3-X (Ø) & 1-X (G))				
	U = NUMBER OF PARALLEL RUNS	MEDIUM VOLTAGE STARTER	MOTOR STARTER/DRIVES:		\vdash
a = CIRCUIT DESIGNATION b = MOUNTING HEIGHT	MULTI CONDUCTOR CABLES K/2/C#16S		b VFD-6 = 6-PULSE VFD VFD-18 = 18-PULSE VFD RVSS = REDUCED VOLTAGE SOLID		
E LUMINAIRE, SURFACE OR PENDANT MOUNTED Has a = CIRCUIT DESIGNATION b = MOUNTING HEIGHT	K (WHERE INDICATED) = NUMBER OF PAIRS 2/C#16S = TWO CONDUCTOR, 16 GAUGE, TWISTED SHIELDED PAIR		a STATE STARTER RVAT = REDUCED VOLTAGE AUTO TRANSFORMER a/B = DEVICE WITH BYPASS		E
	K/3/C#16S K (WHERE INDICATED) = NUMBER OF TRIPLETS 3/C#16S = THREE CONDUCTOR, 16 GAUGE, TWISTED			 	
LUMINAIRE, FLOOD/SPOT ← ← ← LUMINAIRE, FLOOD/SPOT ♡ © (2) SMOKE DETECTOR	SHIELDED TKIPLETS N/CX N = NUMBER OF CONDUCTORS IN THE CARLE		b = INPUT OPTIONS LL = LINE REACTOR PHF = PASSIVE HARMONIC FILTER	SPD SURGE PROTECTIVE DEVICE	
LUMINAIRE, EXIT ONE OR TWO FACES AS INDICATED. ARROW POINTS IN DIRECTION OF EGRESS. ARROW POINTS IN DIRECTION OF EGRESS. P = PHOTOELECTRIC P = PHOTOELECTRIC	X = SIZE OF CONDUCTORS		c = OUTPUT OPTIONS LR = LOAD REACTOR DV/DT = Dv/dt FII TFR	DRAWOUT CONNECTION	
	FIBER OPTIC CABLES		SWF = SINE WAVE FILTER		
	N = NUMBER OF INDIVIDUAL FIBERS				F
	GROUNDING			' - → BATTERY	
	UNDERGROUND GROUND CABLE #4/0 SDBC UNLESS OTHERWISE NOTED				
	GROUND ROD GROUND ROD AND GROUND WELL			LOAD BANK	
F = FLOW SWITCH T = TAMPER SWITCH					
			MANATEE COUNTY	VERIFY SCALES JOB NO.	
SUBMITTAL DRAWN DRAWN CE		Manatee	SEWRF ELECTRICAL MASTE	R PLAN BAR IS ONE INCH ON ORIGINAL DRAWING DRAWING NO	<u>.</u>
CHECKED CE	Car		ELECTRICAL	0	1
REV DATE DATE 1 2 3 4	5 6 7			THIS SHEET, ADJUST SCALES ACCORDINGLY OF XX	x
Ι Ζ Ι Ζ Ι 4 PRO JECT NO. 10006N 00 FILE NAME: 10006N0000CE001 dop 3 4 <		0 9		12 13	

		1 2		3 1	1	5	6	7	g	0		10 14	40	40	
[AB	BREVIA		0	1	8	9		POWER DEVIC		<u> 13</u>	
	A ABS	AMP ABSOLUTE	J	JUNCTION BOX	SWGR SYM	SWITCHGEAR SYMMECTRICAL				1 2	MASTER ELEMENT TIME-DELAY STARTING	OR CLOSING RELAY	83 AUTOMATIC SELECTIVE CO 84 OPERATING MECHANISM	ITROL OR TRANSFER REL	ΑY
7481	AC ACK	ALTERNATING CURRENT ACKNOWLEDGE	K KA	KEY INTERLOCK KILOAMP	TACH TB - X	TACHOMETER TERMINAL BLOCK - UNIT X				3 4	CHECKING OR INTERLO MASTER CONTACTOR	DCKING RELAY	85 PILOT COMMUNICATIONS, C 86 LOCKOUT RELAY	ARRIER OR PILOT-WIRE R	ELAY
<u> </u>	ACTR AF		KV KVA	KILOVOLT KILOVOLT AMPERE	TC TD	THERMOCOUPLE / TIME CLOCK / TRAY TEMPERATURE DETECTOR RELAY	CABLE			5	STOPPING DEVICE STARTING CIRCUIT BRE	EAKER	87 DIFFERENTIAL PROTECTIVE 88 AUXILIARY MOTOR OR MOT	RELAY OR GENERATOR	
ξA		AUTOMATIC FREQUENCY CONTROL AMP INTERRUPTING CAPACITY	KVAR KW	KILOVAR (REACTANCE) KILOWATT	TEFC	TOTALLY ENCLOSED TOTALLY ENCLOSED FAN COOLED	х.			8	ANODE CIRCUIT BREAK	KER CONNECTING DEVICE	89 LINE SWITCH 90 REGULATING DEVICE		A
		AMMETER ANNUNCIATOR ANTENNA	KWD	KILOWATT DEMAND KILOWATT HOUR	TERM	TOTALLY ENCLOSED NON-VENTILATEL TERMINAL)			9 10	UNIT SEQUENCE SWITC	CH	91 VOLTAGE DIRECTIONAL REI 92 VOLTAGE AND POWER DIRE		
-12	APU		L L-B		TM	THERMAL MAGNETIC				12	OVER-SPEED DEVICE		94 TRIPPING OR TRIP-FREE RE	_AY	
Date:	AS	AMMETER SWITCH ASYMMETRICAL	L-G	LINE-GROUND	TS TS1W	TEMPERATURE SWITCH	WINDING			14	UNDER-SPEED DEVICE				
	AT ATO	AMP TRIP AUTOMATIC THROW OVER	LBL	LABEL LIGHTING CONTACTOR	TS2W TSTAT	TWO SPEED SEPARATE WINDING THERMOSTAT				16 17	DATA COMMUNICATION SHUNTING OR DISCHAR	NS DEVICE RGE SWITCH	POWER DEVICE FUNCTION N	IMBERS	_
	ATP ATS	AMMETER TEST POINT AUTOMATIC TRANSFER SWITCH	LCP- X LP	LOCAL CONTROL PANEL NO. X LIGHT POLE	UHF	ULTRA HIGH FREQUENCY				18 19	ACCELERATING OR DEC STARTING-TO-RUNNING	CELERATING DEVICE G TRANSITION CONTACTOR	A ALARM ONLY		
	AUTO XFMF AUX	R AUTOMATIC TRANSFORMER AUXILIARY	LR LTG	LEAD-LAG LOAD REACTOR LIGHTING	UNG UPS	UNGROUNDED UNINTERRUPTABLE POWER SUPPLY				20 21	ELECTRICALLY OPERAT	TED VALVE	B BUS PROTECTION G GROUND FAULT PROTECTION		
	AWG	AMERICAN WIRE GAGE	LV LVL	LOW VOLTAGE LEVEL	UVR	UNDER VOLTAGE RELAY				22 23	EQUALIZER CIRCUIT BR TEMPERATURE CONTRO	REAKER IOL DEVICE	(RELAY CT IN A SYSTEM NEU GS GROUND FAULT PROTECTION	RAL CIRCUIT OR GENERA	TOR PROTECTION)
в	B BAT	BELL BATTERY	M-X	MOTOR CONTROLLER NO. X	V VA	VOLT VOLT AMPERE				24 25	VOLTS PER HERTZ REL SYNCHRONIZING OR SY	.AY YNCHRONISM-CHECK DEVICE		ROUND SENSOR TYPE)	F
	BFG BHP	BELOW FINISHED GRADE BRAKE HORSEPOWER	MA MCA	MILLIAMPERE MOTOR CIRCUIT AMPS	VAR VCP	VARMETER VENDOR CONTROL PANEL				26 27	APPARATUS THERMAL	DEVICE Y	N GROUND FAULT PROTECTION		
hepar	BRF	BREAKER BELOW RAISED FLOOR	MCC - X MCP	MOTOR CONTROL CENTER NO. X MOTOR CIRCUIT PROTECTOR	VED	VARIABLE FREQUENCY DRIVE VERY HIGH FREQUENCY				27N 28	GROUND FAULT UNDER	RVOLTAGE RELAY	T TRANSFORMER PROTECTION		
er: bs	C		MLO	MAINHOLE / MOUNTING HEIGHT MAIN LUGS ONLY MOTOR OPERATED DAMBER	VM VP					29 30	ANNUNCIATOR RELAY		P PHASE PROTECTION		
Š	CCTV	CLOSED CIRCUIT TELEVISION	MOV	MOTOR OFERATED DAMPER	VS	VOLTAGE REGULATOR VOLTAGE SWITCH				32	DIRECTIONAL POWER F	RELAY			
	CKT COAX	CIRCUIT COAXIAL CABLE	MS-X MSP	MOTOR STARTER NO. X MOTOR STARTING PANEL	VTP	VOLTAGE TEST POINT				34 35	MASTER SEQUENCE DE	EVICE			
	COM	COMMON	MTO MTR-X	MANUAL THROW OVER MOTOR NO. X	W WT	WATT / WEST WATER TIGHT				36 37	POLARITY DEVICE		CLK - CLOCK OR TIMING SOURCE		
	CPT CS	CONTROL POWER TRANSFORMER CONTROL SWITCH	MTS MV	MANUAL TRANSFER SWITCH MEGAVOLT	WP	WEATHER PROOF				38 39	BEARING PROTECTIVE	DEVICE DN MONITOR	DFR - DIGITAL FAULT RECORDER	JORDER	
	CT CV	CURRENT TRANSFORMER CONTROL VALVE	MVA MVS	MEGAVOLT-AMPERES MEDIUM VOLTAGE SWITCH	XFMR	TRANSFORMER				40 41	FIELD RELAY FIELD CIRCUIT BREAKE	R	HIZ - HIGH IMPEDANCE FAULT DE	ECTOR	
	CW	CLOCKWISE / COOL WHITE	MW	MEGAWATT						42 43	RUNNING CIRCUIT BREA	AKER R SELECTOR DEVICE	HST - HISTORIAN LGC - SCHEME LOGIC		
	DC DCS	DIRECT CURRENT DISTRIBUTED CONTROL SYSTEM	N NC	NEUTRAL NORMALLY CLOSED						44 45	UNIT SEQUENCE START ABNORMAL ATMOSPHE	TING RELAY RIC CONDITION MONITOR	MET - SUBSTATION METERING PDC - PHASOR DATA CONCENTRA	TOR	
	DCU - X DEMO	DISTRIBUTED CONTROL UNIT NO. X DEMOLITION DISCONNECT SWITCH	NEC	NATIONAL ELECTRICAL CODE NONMETALLIC FLEXIBLE CONDUIT						46 47	REVERSE-PHASE OR BA	ALANCE CURRENT RELAY HASE-SEQUENCE VOLTAGE RELAY	PMU - PHASOR MEASUREMENT UN PQM - POWER QUALITY MONITOR	IT	
	DISC DM		NL NO	NIGHT LIGHT NORMALLY OPEN NAMERI ATE						48 49	MACHINE OR TRANSFO	CE RELAY ORMER THERMAL RELAY	RIO - REMOTE I/O DEVICE RTU - REMOTE TELEMETRY UNIT/F	EMOTE TERMINAL UNIT	
	DPST	DOUBLE POLE SINGLE THROW DOUBLE POLE SINGLE THROW DOOR SWITCH	0							50	AC TIME OVERCURREN	IT RELAY	SER - SEQUENCE OF EVENTS REC TCM - TRIP CIRCUIT MONITOR	ORDER	
	E/G	EMERGENCY GENERATOR	OH OI	OVERIOAD RELAY						53	FIELD EXCITATION REL				
	EM EMT		P	POLE						55 56	POWER FACTOR RELAY				
	ENCL	ENCLOSURE	PA PANEL I	PUBLIC ADDRESS						57	SHORT-CIRCUITING OR	R GROUNDING DEVICE			
P	ENT EP	ELECTRICAL NON-METALLIC TUBING EXPLOSION PROOF	PANEL-F PB	PX POWER DISTRIBUTION PANEL NO. X PUSHBUTTON / PULL BOX						59 60	OVERVOLTAGE RELAY	T BALANCE RELAY			
5	ETM	ELAPSED TIME METER	PC-X PCS	MINI POWER CENTER NO. X PVC COATED GALVANIZED STEEL CONDUIT						61 62	DENSITY SWITCH OR SE TIME-DELAY STOPPING	ENSOR OR OPENING RELAY			
cale:	FA FACP	FIRE ALARM FIRE ALARM CONTROL PANEL	PCM PE	PROCESS CONTROL MODULE PHOTOCELL						63 64	PRESSURE SWITCH GROUND DETECTOR RE	ELAY			
Plots	FDR FLA	FEEDER FULL LOAD AMPS	PF PFCC	POWER FACTOR POWER FACTOR CORRECTION CAPACITOR						65 66	GOVERNOR NOTCHING OR JOGGINO	G DEVICE			
ben	FLX FO		PFR PH	PHASE FAILURE RELAY PHASE						67 68	AC DIRECTIONAL OVER BLOCKING OR OUT OF S	RCURRENT RELAY STEP RELAY			-
0905	FREQ	FIBERGLASS RIGID CONDOL FREQUENCY ELISE	PNL PPX	PANEL POWER PANEL NO. X						69 70	RHEOSTAT	DEVICE			
- -	FU	SW FUSED SWITCH	PT	POTENTIAL TRANSFORMER POLYVINYL CHLORIDE RIGID PLASTIC CONDI	шт					72	DC CIRCUIT BREAKER	ACTOR			
PF.	FVR FWD	FULL VOLTAGE REVERSING FORWARD	PWR	POWER						74	ALARM RELAY POSITION CHANGING M	IECHANISM			
E	G	GROUND / EQUIPMENT GROUND / GROUND FAULT	RAC RECPT	RIGID ALUMINUM CONDUIT RECEPTACLE						76 77	DC OVERCURRENT REL TELEMETERING DEVICE	LAY E			E
DI DI	GEN GRC	GENERATOR GALVANIZED STEEL RIGID CONDUIT	REV RF	REVERSE RADIO FREQUENCY						78 79	PHASE-ANGLE MEASUR AC RECLOSING RELAY	RING RELAY			
gnscr	GFCI GFI	GROUND FAULT CIRCUIT INTERRUPTER (RECEPTACLE) GROUND FAULT INTERRUPTER (BREAKER)	RMS RVAT	ROOT MEAN SQUARED REDUCED VOLTAGE AUTO TRANSFORMER						80 81	FLOW SWITCH FREQUENCY RELAY				
Desi	GFR		RVNR RVSS	REDUCED VOLTAGE NON-REVERSING REDUCED VOLTAGE SOLID STATE						82	DC LOAD MEASURING F	RECLOSING RELAY			
	H HF HP		S	SHIELD / SHORT-TIME											-
Jshadi	HPS	HIGH PRESSURE SODIUM HOUR	SC SDBC	SHORT CIRCUIT SOFT DRAWN BARE COPPER											
Die: C	HSTAT HV	HUMIDISTAT HIGH VOLTAGE	SFL												
olor la	HVAC HZ	HEATING/VENTILATION/AIR CONDITIONING HERTZ	SM	SURFACE MOUNTED SINGLE POLE											
۲ F	I	INSTANTANEOUS LOAD	SPD SPDT	SURGE PROTECTIVE DEVICE SINGLE POLE DOUBLE THROW											F
ayout	IC IJB	INTERRUPTING CAPACITY INSTRUMENT JUNCTION BOX	SPST SPKR	SINGLE POLE SINGLE THROW SPEAKER											
	IMC INST	INTERMEDIATE METAL CONDUIT INSTANTANEOUS	SS STB	SOLID STATE SHORTING TERMINAL BLOCK											
ق	INT INTERCOM	INTERLOCK INTERCOMMUNICATION	SW SWBD	SWITCH SWITCHBOARD											
Н															-
	NOTES:														
	1. REFER TO	O SPECIFICATIONS AND OTHER DRAWINGS FOR ADDITIONA	AL ABBREV	IATIONS.											
G		PRELIMINARY DESIG	GN	DESIGNED CE					164			MANATEE COU	JNTY	VERIFY SCALES	JOB NO. 10096N.00
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							C C A	rollo	Man	atee		ELECTRICAL		0 1"	00GE02
Ne -				CE					FLORI			ABBREVIATI	ONS	IF NOT ONE INCH ON	SHEET NO.

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MANATEE COUNTY			JOB NO. 10096N.00	G
VRF ELECTRICAL MASTER ELECTRICAL SWGR-1A/2B ONE-LINE DIAGRAM	2 PLAN	DAR IS UNE INCH ON ORIGINAL DRAWING 0 1" IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY	DRAWING NO. 03E01 SHEET NO. OF XX	
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MANATEE COUNTY	VERIFY SCALES	JOB NO. 10096N.00	G	
VRF ELECTRICAL MASTER	BAR IS ONE INCH ON ORIGINAL DRAWING			
ELECTRICAL		0 1"	03E04	
MCC-1A		IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.	
ONE-LINE DIAGRAM		SCALES ACCORDINGLY	OF XX	
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	MCC-2	MCC-2								
C	NE-LINE DIAGRAM									
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MOTOR METERING PUMP 1	METERING PUMP 2			_
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MANATEE COUNTY		VERIFY SCALES	JOB NO. 10096N.00	G
WRF ELECTRICAL MASTER	R PLAN	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.	
ELECTRICAL		0 1"	03E06	
	1	IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGI Y	SHEET NO.	
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MANATEE CO VRF ELECTRICAL ELECTRIC MCC-4 ONE-LINE DI 11	OUNTY MASTER PLAN AL H AGRAM	12	VERIFY SCALES BAR IS ONE INCH ON ORIGINAL DRAWING 0 1 1" IF NOT ONE INCH ON THIS SHEET. ADJUST SCALES ACCORDINGLY 13	JOB NO. 10096N.00 DRAWING NO. 03E08 SHEET NO. OF XX	G


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MANATEE COUNTY		VERIFY SCALES	JOB NO. 10096N.00	G
VRF ELECTRICAL MASTE	R PLAN	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.	
ELECTRICAL		0 1"	03E10	
MCC-5		IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.	
ONE-LINE DIAGRAM	1 – 11	SCALES ACCORDINGLY	OF XX	
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MANATEE COUNTY		VERIFY SCALES	JOB NO. 10096N.00	G
VRF ELECTRICAL MAST	ER PLAN	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.	
ELECTRICAL		0 1"	03E12	Í
MCC-6	IF NOT ONE INCH ON THIS SHEET ADJUST	SHEET NO.		
ONE-LINE DIAGRAM - II		SCALES ACCORDINGLY	OF XX	
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VRF ELECTRICAL MASTER PLAN			BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.	
	ELECTRICAL		0 1"	03E15	
	MCC-9		IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.	
0	NE-LINE DIAGRAM		SCALES ACCORDINGLY	OF XX	
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MANATEE COUNTY VERIFY SCALES JOB NO. 10096N.00 VRF ELECTRICAL MASTER PLAN BARE ONE NOL HOL 00096N.00 DRAWING NO. 03E16 VRF ELECTRICAL MCC-10 0 11 MCC-10 FAOTONE NOL HOL 000000000000000000000000000000000000						D
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MANATEE COUNTY VERIFY SCALES JOB NO. 10096N.00 JOB NO. WRF ELECTRICAL MASTER PLAN BAR IS ONE INCH ON ORIGINAL DRAWING DRAWING NO. ELECTRICAL 0 0 MCC-10 If NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY SHEET NO. 0 0F XX 0F XX						F
MANATEE COUNTY VERIFY SCALES JOB NO. 10096N.00 JOB NO. 10096N.00 JOB NO. NRF ELECTRICAL MASTER PLAN BAR IS ONE INCH ON ORIGINAL DRAWING DRAWING NO. DRAWING NO. ELECTRICAL 0 TI 0 SHEET NO. MCC-10 If NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY SHEET NO. OF XX 11 12 13						
MANATEE COUNTY VERIFY SCALES JOB NO. 10096N.00 JOB NO. 10096N.00 G NRF ELECTRICAL MASTER PLAN 0 DRAWING NO. 03E16 ELECTRICAL 0 03E16 SHEET NO. MCC-10 IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY SHEET NO. 11 12 13						
MANATEE COUNTY VERIFY SCALES JOBEND. 10096N.00 G WRF ELECTRICAL MASTER PLAN DRAWING NO. DRAWING NO. ELECTRICAL 0 0 0 MCC-10 IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY SHEET NO. 11 12 13						
Image: Non-angle of the second sec				VERIFY SCALES BAR IS ONE INCH ON	10096N.00	G
MCC-10 IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY SHEET NO. 11 12 13	WKFE				03E16	
OINE-LINE DIAGRAIVI Surger and the surger	^			IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.	
			12	13	OF XX	'



FILE NAME: 10096N0003E017.dgn



11	12	13	
		12 SEE SHEET 03E16	
	PROM MCC	12. SEE SHEET USE 10.	
	2 INCLUDES E	BYPASS.	
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N	IANATEE COUNTY		VERIFY SCALES	JOB NO. 10096N.00
VRF E	LECTRICAL MASTER	R PLAN	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.
	ELECTRICAL		0 1"	03E18
	MCC-11A		F NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.
0	NE-LINE DIAGRAM	-	SCALES ACCORDINGLY	OF XX
	11	12	13	





	D. 10096N.00	FILE NAME:	10096N0003E02
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11	12	13
	KEY NOTES:	E18.
	2 INCLUDES BYPASS.	

MANA	TEE COUNTY		VERIFY SCALES	JOB NO. 10096N.00
F ELECT	RICAL MASTER	R PLAN	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.
	ELECTRICAL		0 1"	03E20
Ν	/ICC-12		IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.
ONE-L	INE DIAGRAN	-	SCALES ACCORDINGLY	OF XX
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epard N		DESIGNED			
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AST SAVED BY: bshepard M	3 PRELIMINARY DESIGN SUBMITTAL NOT FOR CONSTRUCTION	DESIGNED AHR DRAWN SMB CHECKED DATE MAY 2017	Ccarolic	* Manatee County FLORIDA	SE



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Μ	IANATEE COUNTY	VERIFY SCALES	JOB NO. 10096N.00	G	
VRF E	LECTRICAL MASTER	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.		
	ELECTRICAL	0 1"	03E21		
	MCC-13	IF NOT ONE INCH ON THIS SHEET, ADJUST	SHEET NO.		
٨O	NE-LINE DIAGRAM	SCALES ACCORDINGLY	OF XX		
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MANATEE COUNTY	VERIFY SCALES	JOB NO. 10096N.00	G	
EWRF ELECTRICAL MASTE	BAR IS ONE INCH ON ORIGINAL DRAWING	DRAWING NO.		
	0 1"	03E22	1	
ELECTRICAL		OULLL	1	
MCC-14		IF NOT ONE INCH ON	SHEET NO.	Í
ONE-LINE DIAGRAM	SCALES ACCORDINGLY	OF XX		
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PROJECT NO. 10096N.00 FILE NAME: 10096N0003E024.dgn



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DESCRIPTION

MAY 2017

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MANATEE NRF ELECTRIC ELEC MCC ONE-LINE	E COUNTY CAL MASTER TRICAL -SEP E DIAGRAM	2 PLAN	VERIFY SCALES BAR IS ONE INCH ON ORIGINAL DRAWING 0 1 11 IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY 13	JOB NO. 10096N.00 DRAWING NO. 03E25 SHEET NO. OF XX	G